Climate Resilience Design Standards and Guidance – Compiled Downloadable Methods PDFs Version 1.4, December 2024

CLIMATE RESILIENCE DESIGN STANDARDS

TIERED METHODS TO CALCULATE DESIGN CRITERIA VALUES

Version 1.4 DECEMBER 2024



CLIMATE RESILIENCE DESIGN STANDARDS

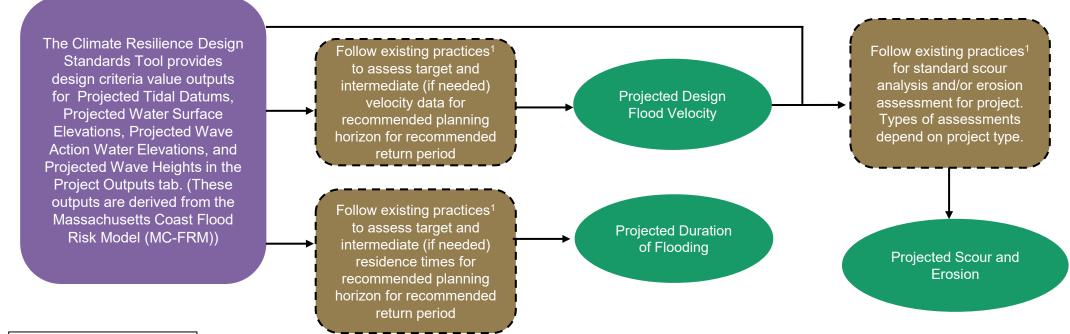
PROJECTED SEA LEVEL RISE / STORM SURGE DESIGN CRITERIA METHODS ALL TIERS

Version 1.4 DECEMBER 2024



Method to Assess Projected Sea Level Rise / Storm Surge Design Criteria

Given Standards Output from Tool: Planning Horizon (2030, 2050, 2070); Return Period [Annual Exceedance Probability] (20-yr [5%], 50-yr [2%], 100yr [1%], 200-yr [0.5%], 500-yr [0.2%], 1000-yr [0.1%])



 Consult a professional coastal engineer or scientist/modeler to estimate projected Duration of Flooding, Design Flood Velocity, and Scour & Erosion based on the recommended Standards and outputs provided through this Tool.

Legends Tool Output Calculation steps Design Criteria Existing practice **CLIMATE RESILIENCE DESIGN STANDARDS**

PROJECTED TOTAL PRECIPITATION DEPTH DESIGN CRITERIA

TIERED METHODOLOGY

Tier 3 Dams and Flood Control Structure Projects – Pages 2-15

Tier 1 Projects – Pages 16-17

Version 1.4

DECEMBER 2024



Given Standards Output from Tool: Planning Horizon (2030, 2050, 2070); Return Period (5-yr, 10-yr, 25-yr, 50-yr, 100-yr, 200-yr, 500-yr)

Download daily precipitation projections for RCP 8.5 scenario from LOCA¹ dataset (<u>Draft-SOP-Datadownload-</u> <u>LOCA.pptx</u>) using 14 Group1² Global Climate Models (GCMs) for the grid(s) corresponding to the project location

Repeat the same steps for two more grids around the project location (a total of 3 grids from each location). Avoid grids that contains more than 1/3rd of water body

Choose 30-yr averaging period around given planning horizon

Calculate annual maximum rainfall for each year for each grid in the 30-yr averaging period per GCM Fit Generalized Extreme Value (GEV) distribution to the annual maxima to calculate modeled baseline and modeled future projections for given planning horizon and given return period for each GCM per grid

Convert the 1-day design storm depths to 24-hour design storm depths using factor 1.11³ per GCM per grid

Calculate the ratios between modeled baseline and modeled future per GCM per grid

Calculate mean, 5%CL and 95% CL of the ratios between modeled baseline and modeled future for all GCMs and apply that to NOAA Atlas 14 median values⁴ to estimate the projected 24-hour precipitation depths for given return period for each

grid

Calculate mean of the projected 24-hour precipitation depths for all grids

Projected Total Precipitation Depth for 24-hr Design Storm for given planning horizons and given return period*

* Tier 3 Dams and Flood Control Structures will also receive output from the Tool and an Attention note to compare the calculated depth using the methodology shown in this figure with the Tool output.

- Pierce, D.W., D.R. Cayan, and B.L. Thrasher, Statistical Downscaling Using Localized Constructed Analogs (LOCA). Journal of Hydrometeorology, 2014. 15(6): p. 2558-2585
- Applying Climate Change Information to Hydrologic and Coastal Design of Transportation Infrastructure (NCHRP Project 15-61- Final Report) by Kilgore et al., 2019
- 3. NOAA Atlas 14 Precipitation Frequency Estimates: Northeastern States; NOAA Atlas 14, Volume 10, Version 3

Data Gathering Calculation steps Design Criteria Existing practice

Legends

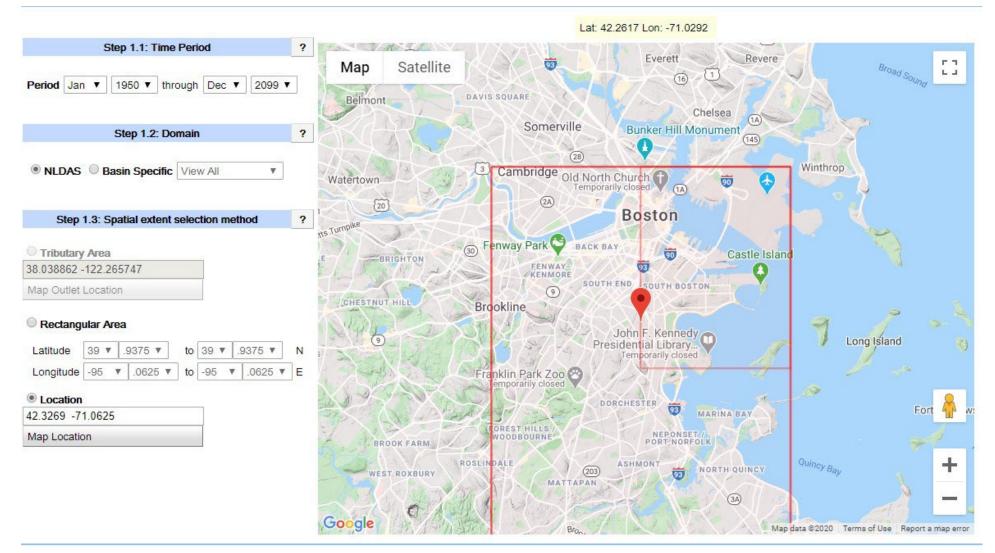
Tiered Methodology to Assess Projected Total Precipitation Depth for 24-hr Design Storm Tier 3 - Dams and Flood Control Structures (Step 0: Download LOCA Dataset)

	 Go to https://gdo-dcp.ucllnl.org/ Go to page "Projection: Subset F 		
STEP 1 Go to sub-tab "Page 1. Temporal & Spatial Extent"	STEP 2 Go to sub-tab "Page 2. Products, Variables, Projections"	STEP 3 Go to sub-tab "Page 3. Analysis, Format, and Notification"	STEP 4 Data request and data download
Step 0.1.1 : "Time Step and Period", select daily period from Jan-1950 through Dec-2099	Step 0.2.4: "Select Projection Sets", check "LOCA-CMIP5-Climate-daily"	Step 0.3.7: "Analysis", keep dial set to "No Analysis"	Step0.4.1:Pressbutton"Submit Request" on top leftStep0.4.2:A popup box will
Step 0.1.2: "Domain", select	Step 0.2.5: Under "Products" select both "1/16 degree" boxes. For	Step 0.3.8: " Output Format", choose "ASCII text, comma- delimited (csv)"	appear with details of the submission. Press "Submit". Press "Ok".
'NLDAS" Step 0.1.3: Select "Location" method and either enter the	"Variables", check "Precipitation Rate (mm/dd)" Step 0.2.6 : Under "Emissions	Step 0.3.9 : "Notification when Processing is Complete", enter your email address twice.	Step 0.4.3 : Click on the link that arrives in the email a few hours later to get to an ftp directory of files produced for your job request
latitude, longitude pair OR specify interactively within the map based on Project Location. If the selected grid includes more than 1/3 rd water body, also download data from the adjacent grid.	Scenarios, Climate Models and Runs", check boxes associated with Group 1 GCMs per NHCRP15-61 report ¹ , as shown in the Step 2.6 example slide. For each model, select emission scenario RCP8.5 for precipitation.	Finally, check your user type, application type, and applicable resource area(s) as appropriate.	Step 0.4.5 : Click folder "Loca5" and download the .csv file for the climate projection data and .txt files for data related information
		REFERENCES	

1. Applying Climate Change Information to Hydrologic and Coastal Design of Transportation

Infrastructure (NCHRP Project 15-61- Final Report) by Kilgore et al., 2019

Download LOCA Dataset (Example: Project Area and Time Selection) Moakley Park, South Boston, MA



Download LOCA Dataset (Example: Projection Set and Variables Selection) Moakley Park, South Boston, MA

Submit Request			s (completed == gre 3 2.4 2.5 2.6 3.7			:	Size (%, 100 max): 6	
Page 1: Temporal &	Spatial Extent	Page 2: Products, Varial	oles, Projections	Page 3: Analysis, Fo	rmat, & Notification			
		Step 2.4: Selec	ct Projection Set (G	reen text indicates pro	ojection set form comp	leted)		
		BC	SD-CMIP3-Climate- CAv2-CMIP3-Clima SD-CMIP3-Hydrolog	te-daily BCCA gy-monthly BCSD	-CMIP5-Climate-month v2-CMIP5-Climate-dail -CMIP5-Hydrology-mor -CMIP5-Climate-daily	y		
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			Step 2.5: Produc	ts & Variables daily	projections			?
		🗹 1/16 degi	ree LOCA projection ree Observed data (LOCA projections	1950-2005) 🔲 Min Su	itation Rate (mm/day) ırface Air Temperature urface Air Temperature			

Download LOCA Dataset (Example: Group1* GCM Selections for Emission Scenario RCP8.5) Moakley Park, South Boston, MA

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Check the Following Boxes under RCP8.5:

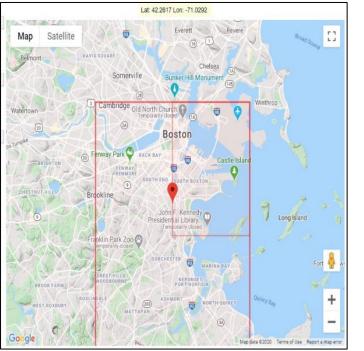
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- ✓ bcc-csm-1-m
- ✓ ccsm4
- ✓ cnrm-cm5
- ✓ csiro-mk3-6-0
- ✓ gfdl-cm3
- ✓ giss-e2-h

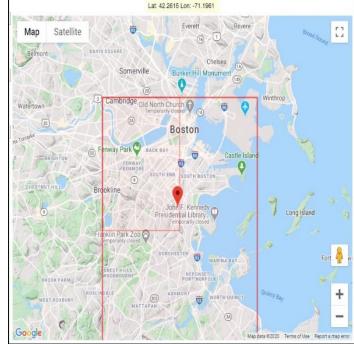
- ✓ giss-e2-r
- ✓ hadgem2-ao
- ✓ hadgem2-cc
- ✓ inmcm4
- ✓ ipsl-cm5a-lr
- ✓ miroc5
- ✓ mri-cgcm3

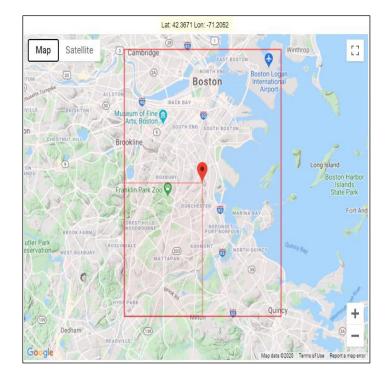
Download LOCA Dataset (Example: Type of Analysis, Output Format, and Others) Moakley Park, South Boston, MA

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JaneDoe@mass.gov	Email Address		
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Dostoni rocipartar	Tag/Label for request (Optional, characte	rs may be letters, numbers, or _)	
	Step 3.10: Usage Information		
Please specify usage information	below. This information will help LLNL and Re	clamation track how this archive is	
serving various sectors and entitie	s in the user community. For entity and applie	cation lists, please make one selection.	
For sector, please make one or m	ultiple selections.		
Entity	Application	Sector(s)	
Govt Federal	Research	Water Quantity	
Govt State	Environmental Documentation	Water Quality	
-	/Local O Endangered Species consultation	Flood Management	
Research Institut	,	Energy	
Academic Institu	tion Adaptation Planning	Air Quality	
Private Sector	Other	Ecosystem - Land	
Non-Govt. Organ	nization	Ecosystem - Aquatic	
Other		Social Systems	
		Other	

Tiered Methodology to Assess Projected Total Precipitation Depth for 24-hr Design Storm Tier 3 - Dams and Flood Control Structures (Step 1 Example: Select 2 More Grids Around Project Location to Download LOCA Datasets) Moakley Park, South Boston, MA







(Step 2 – 3 Example: Calculating Annual Maximum for each GCM for each Grid for RCP 8.5 in the 30 Year Span Surrounding Each Planning Horizon*) Moakley Park, South Boston, MA

	Max of bcc-	Max of bcc-	Max of	Max of cnrm-	Max of csiro-	Max of gfdl-	Max of giss-	Max of giss-	iviax ui	IVIAX UI	Max of	Max of ipsl-	Max of	Max of mri-
YEAR	csm1-1.1	csm1-1-m.1	ccsm4.6	cm5.1	mk3-6-0.1	cm3.1	e2-h.6	e2-r.6	hadgem2- ao 1	hadgem2-	inmem4.1	cm5a-Ìr.1	miroc5.1	egem3.1
2060	208.7	170.6	221.6	189.3	317.2	139.8	194.6	171.1	173.6	183.2	154.5	175.5	146.2	128.9
2061	173.0	163.2	157.1	182.5	152.1	125.6	146.5	156.9	160.6	171.5	125.3	169.7	144.3	119.9
2062	111.9	152.9	145.4	151.6	125.8	124.8	127.3	133.6	150.4	122.3	116.4	143.6	140.2	117.3
2063	109.7	135.1	129.2	130.0	119.0	116.1	124.7	114.6	142.2	117.6	112.9	124.2	135.5	107.4
2064	104.9	134.4	120.3	92.5	92.7	109.5	123.4	111.6	118.1	116.2	112.2	97.9	125.4	104.3
2065	92.4	132.1	109.3	92.2	91.3	107.8	110.4	105.9	117.4	109.8	101.8	90.3	117.1	103.8
2066	92.0	124.4	108.8	87.5	90.3	104.0	100.6	99.2	107.9	93.9	100.7	90.1	113.3	91.3
2067	85.6	118.6	99.6	87.1	90.2	96.6	88.5	98.7	102.0	89.9	91.2	89.9	107.9	91.0
2068	85.0	112.8	90.8	86.8	87.3	95.9	88.2	98.3	100.3	87.5	85.8	85.5	103.3	89.9
2069	82.1	111.1	76.8	85.1	83.9	93.1	82.5	87.6	99.3	86.5	75.9	80.9	100.0	88.5
2070	81.8	105.2	74.7	78.6	82.0	91.9	81.7	86.1	98.8	84.6	73.8	80.4	93.7	87.0
2071	73.3	98.7	72.1	78.0	81.9	87.6	80.8	76.5	98.2	79.3	72.4	78.4	88.9	84.5
2072	72.5	91.1	69.9	77.9	79.5	85.9	78.6	69.1	90.0	77.9	71.0	76.3	88.9	78.0
2073	72.2	90.5	68.1	77.6	76.3	80.3	75.6	68.3	87.9	77.1	71.0	72.7	86.8	74.9
2074	69.1	86.3	68.0	71.0	76.2	78.0	74.9	65.4	84.1	75.1	70.6	71.2	81.9	73.2
2075	67.6	82.4	66.3	68.6	75.9	75.1	72.6	64.5	81.8	74.7	70.2	70.8	74.6	73.0
2076	66.9	79.1	66.2	68.1	75.2	74.2	70.5	64.1	76.3	73.6	68.1	69.9	73.7	72.1
2077	66.8	75.4	65.4	67.3	70.7	74.0	66.5	63.8	74.9	73.4	63.1	69.7	70.7	71.3
2078	65.6	74.0	62.6	65.0	70.3	73.2	64.7	62.2	74.4	72.4	61.1	68.8	68.5	66.4
2079	65.1	68.0	61.2	64.3	69.1	73.2	64.6	61.2	74.4	72.3	59.8	68.2	68.2	66.4
2080	64.7	67.7	61.1	60.6	66.9	70.9	61.6	59.5	73.8	67.9	59.3	64.9	66.9	65.3
2081	62.6	67.0	59.0	59.1	66.0	68.9	61.4	59.2	71.8	63.8	58.0	62.9	65.7	65.0
2082	61.3	65.8	57.1	56.6	65.0	68.0	56.0	58.7	62.5	59.0	51.3	62.6	61.4	59.1
2083	60.5	65.1	53.8	54.5	62.1	60.8	55.7	56.5	62.4	58.9	49.0	60.0	60.1	52.3
2084	54.7	64.4	53.6	49.9	61.7	60.2	52.2	56.4	60.3	58.9	47.0	59.1	59.7	51.3
2085	54.7	61.1	51.2	49.4	58.0	56.5	51.2	52.2	56.0	58.5	45.9	54.1	57.8	50.2
2086	50.1	51.4	45.6	47.0	57.4	55.0	50.1	48.3	55.3	56.3	45.5	53.9	54.5	48.9
2087	43.8	49.8	43.4	46.8	53.5	52.5	48.0	47.7	55.1	54.6	45.3	50.4	54.4	46.5
2088	40.9	45.6	40.8	43.8	50.8	50.5	46.4	45.8	51.5	53.6	43.7	44.9	54.1	40.6
2089	28.1	40.4	36.5	41.2	47.8	42.4	44.9	37.5	50.5	46.6	43.0	44.0	50.2	40.1

*This chart shows annual maximums for the 2070s planning horizon only.

(Step 4 Example: Fitting GEV Distribution on annual maxima of each grid for each GCM*) Moakley Park, South Boston, MA

2060 1 207 6.95 6.95 670.61 5.69 5.69 7.73 7.39 7.30 7.37 7.39 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7.30 7	b1 b2 Max of ccsm4.6 b1 b2 Max of cnrm- cm5.1 b1 b2 Max of csiro- mk3-6-0.1 b1 b2	Max of ccsm4.6	b2	Ь1	Max of bcc- csm1-1-m.1	ь2	ы	Max of bcc- csm1-1.1	Bank	Year	
2061 2 173.04 5.57 5.77 153.77 152.85 5.66 177.15 5.06 4.88 182.48 5.87 5.66 187.17 4.90 2062 3 1156.6 3.28 2.33 125.07 4.04 3.60 125.24 3.66 3.45 123.92 3.88 3.47 115.04 3.56 2064 5 52.40 2.25 2.09 112.43 3.68 3.01 2.48 92.67 2.24 2.98 2.99 105.25 2.11 162 90.27 2.28 2066 7 95.59 2.16 162 115.17 3.00 2.26 197.57 8.76 2.00 152 2.09 122.2 2.21 163 90.21 2.28 2.00 152.2 2.01 165 90.21 2.28 133 33.68 133 33.86 133 33.86 133 33.86 133 33.86 133 33.86 133 33.86 133	5.69 5.69 221.58 7.39 7.39 189.26 6.31 6.31 317.22 10.57 10.57	221.58	5.69	5.69	170.61	6.96	6.96	208.71	1	2060	
2063 4 19956 3.28 2.39 135.07 4.04 3.60 123.24 3.86 3.45 129.38 3.87 3.47 190.44 3.56 2065 6 92.40 255 2.09 132.99 3.84 2.99 170.28 3.01 2.48 92.16 2.54 2.09 17.2 2.66 2.84 92.67 2.66 2.84 90.7 2.28 2.26 2.27 2.26 2.28 92.7 2.20 115.2 2.21 1.82 90.7 2.20 116.2 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 116.5 90.7 2.20 128 133 83.66 1.33 20070 11 97.17 12.5 137 76.80 1.77 1.20 138 139	5.25 5.06 157.13 5.06 4.88 182.48 5.87 5.66 152.11 4.90 4.72	157.13	5.06	5.25		5.37		173.04	2		
2064 5 104.53 30.2 2.58 184.39 3.66 3.31 100.34 3.46 2.96 12.48 2.66 2.26 2.26 2.26 2.26 2.26 2.26 2.26 2.26 2.26 2.26 2.25 2.52 2.52 2.52 2.56 107.30 2.48 2.26 3752 2.31 162 90.31 2.38 2066 7 91.95 2.43 191 127.96 2.72 194 9073 2.18 157 2.09 150 97.27 2.11 2069 10 87.12 188 12.08 177 12.0 88.78 2.09 150 97.27 2.11 163 105 78.59 172 10 83.36 133 103 103 83.36 133 103 103 103 83.36 133 103 103 103 103 103 103 103 103 103 103 103 103 10		145.41	4.41		152.89	3.23	3.47	111.94	3	2062	
2065 6 9240 255 209 19278 301 248 92.56 254 209 9126 252 2067 8 9559 216 1127 120 253 188 268 265 97.52 231 182 90.31 238 2068 9 84.88 205 147 112.72 272 194 90.73 219 157 85.78 200 150 97.77 211 2068 10 82.12 188 128 1111 255 173 76.60 177 120 85.12 198 133 83.86 133 2070 11 8181 173 155 203 144 74.77 163 105 77.39 143 07.6 77.59 143 07.6 77.59 143 07.6 77.59 143 07.6 77.59 143 07.6 77.59 143 07.6 77.59 143 07.6<		129.24	3.60	4.04	135.07	2.93	3.28	109.66	4	2063	
$ \begin{bmatrix} 2066 & 7 & 9196 & 243 & 191 & 12436 & 329 & 258 & 10833 & 288 & 226 & 7752 & 231 & 182 & 9031 & 239 \\ 2068 & 9 & 6498 & 206 & 147 & 11278 & 272 & 194 & 9077 & 218 & 157 & 6678 & 209 & 150 & 6727 & 211 \\ 2068 & 10 & 6212 & 188 & 128 & 1111 & 255 & 173 & 7680 & 177 & 120 & 6572 & 196 & 133 & 6326 & 139 \\ 2070 & 11 & 8181 & 173 & 15 & 105.16 & 230 & 148 & 7471 & 163 & 105 & 7853 & 172 & 10 & 8204 & 179 \\ 2071 & 12 & 7329 & 152 & 0.92 & 9877 & 204 & 124 & 7207 & 149 & 0.91 & 7807 & 151 & 0.98 & 139 \\ 20772 & 13 & 7254 & 142 & 0.81 & 9109 & 178 & 102 & 6538 & 137 & 0.78 & 77.91 & 152 & 0.87 & 7551 & 155 \\ 2073 & 14 & 7218 & 133 & 0.71 & 9053 & 166 & 0.89 & 6811 & 125 & 0.67 & 77.55 & 143 & 0.76 & 77.59 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.05 & 122 & 0.17 & 75.99 & 71.00 & 0.43 & 77.39 & 112 & 0.38 & 70.74 & 0.29 & 73.99 & 0.42 & 8077 & 0.20 & 65.99 & 100 & 0.51 & 82.42 & 133 & 0.62 & 66.32 & 107 & 0.58 & 8077 & 102 & 0.44 & 75.20 & 112 & 2076 & 17 & 66.77 & 0.06 & 77.39 & 0.75 & 0.76 & 0.75 & 0.24 & 67.99 & 0.75 & 0.26 & 66.32 & 107 & 0.58 & 67.33 & 0.33 & 0.38 & 70.74 & 0.29 & 122 & 2076 & 118 & 0.07 & 0.25 & 6116 & 0.70 & 0.23 & 65.07 & 0.02 & 0.37 & 73.97 & 0.75 & 0.53 & 0.11 & 65.79 & 0.23 & 0.65 & 0.53 & 0.13 & 0.75 & 0.75 & 0.70 & 0.26 & 65.73 & 0.07 & 0.26 & 65.73 & 0.07 & 0.$				3.86		2.58			5	2064	
$ \begin{bmatrix} 2067 & 8 & \frac{8559}{206} & 2.66 & 162 & \frac{116}{2} & \frac{112}{102} & \frac{112}{28} & \frac{300}{272} & 2.25 & \frac{9963}{979} & 2.52 & 189 & \frac{8707}{77} & 2.20 & 165 & \frac{9927}{72} & 2.28 \\ 2083 & 10 & \frac{8212}{2} & 188 & 1.28 & \frac{1111}{111} & 255 & 173 & \frac{78.80}{78.0} & 177 & 120 & \frac{85.78}{75} & 2.09 & 150 & \frac{8727}{72} & 2.11 \\ 2070 & 11 & \frac{8181}{732} & 172 & 0.52 & \frac{99671}{202} & 2.24 & \frac{144}{771} & \frac{77.71}{163} & 1.05 & \frac{78.59}{78.59} & 1.72 & 110 & \frac{82.04}{77.91} & 173 \\ 2071 & 12 & \frac{73.29}{732} & 152 & 0.92 & \frac{99.71}{98.71} & 2.04 & 124 & \frac{77.71}{72.04} & 143 & 0.51 & \frac{78.59}{77.91} & 152 & 0.87 & \frac{79.51}{79.55} & 143 \\ 2072 & 13 & \frac{72.54}{72.18} & 142 & 0.81 & \frac{91.09}{91.09} & 178 & 102 & \frac{88.88}{988} & 137 & 0.78 & \frac{77.91}{77.91} & 152 & 0.87 & \frac{79.51}{79.55} & 145 \\ 2073 & 14 & \frac{72.18}{72.18} & 133 & 0.71 & \frac{90.53}{90.53} & 166 & 0.89 & \frac{68.81}{98.81} & 125 & 0.77.91 & 152 & 0.87 & \frac{79.51}{79.55} & 143 \\ 2076 & 17 & \frac{66.87}{100} & 0.51 & \frac{82.42}{133} & 162 & \frac{66.32}{149} & \frac{107}{10.59} & \frac{88.07}{7.95} & 112 & 0.61 & \frac{76.24}{75.86} & 113 \\ 2076 & 17 & \frac{66.87}{100} & 0.43 & \frac{73.59}{73.5} & 104 & 0.44 & \frac{65.14}{10.99} & 0.39 & 0.42 & \frac{88.07}{10.2} & 100 & 0.51 & \frac{75.89}{75.89} & 122 \\ 2076 & 17 & \frac{65.78}{100} & 0.51 & \frac{87.99}{73.5} & 118 & 0.51 & \frac{65.21}{65.22} & 107 & 0.50 & \frac{88.07}{10.2} & 100 & 0.51 & \frac{75.89}{75.89} & 122 \\ 2078 & 19 & \frac{65.78}{9} & 0.22 & 0.36 & \frac{75.39}{73.99} & 0.44 & 0.33 & \frac{65.74}{65.44} & 0.99 & 0.35 & \frac{67.33}{67.33} & 0.38 & \frac{70.74}{70.74} & 0.88 \\ 2079 & 20 & \frac{65.08}{0.07} & 0.75 & 0.24 & \frac{67.99}{0.79} & 0.78 & 0.25 & \overline{6115} & 0.70 & 0.23 & \overline{64.27} & 0.74 & 0.24 & \overline{6315} & 0.79 \\ 2080 & 21 & \frac{64.67}{7} & 0.67 & 0.19 & \frac{67.89}{0.75} & 0.53 & 0.11 & 0.63 & 0.18 & \overline{60.55} & 0.63 & 0.18 & \overline{66.86} & 0.69 \\ 2081 & 22 & \overline{65.05} & 0.44 & 0.07 & \overline{65.08} & 0.76 & 0.25 & \overline{6115} & 0.77 & 0.46 & 0.10 & \overline{55.61} & 0.44 & 0.10 & \overline{55.03} & 0.52 \\ 2086 & 27 & \overline{50.06} & 0.77 & 0.57 & 0.53 & 0.11 & 0.00 & \overline{53.47} & 0.22 \\ 2086 & 27 & \overline{50.07} & 0.00 & $	3.64 2.99 109.28 3.01 2.48 92.16 2.54 2.09 91.25 2.52 2.07		2.99						6	2065	
2068 9 84.38 205 147 117.278 272 194 90.79 2.19 157 86.78 2.09 150 87.77 2.11 2070 11 8181 179 125 105.16 2.30 148 74.71 163 105 78.99 1.72 110 82.04 179 2071 12 73.23 152 0.92 38.71 2.04 124 72.07 149 0.91 77.89 172 10 82.04 179 2072 13 72.24 142 0.81 91.09 178 102 86.81 137 0.78 77.91 152 0.87 755.1 155 2073 14 72.18 133 0.71 90.53 166 0.89 83.11 1.25 0.67 77.99 143 0.76 76.22 1.40 2075 16 67.55 109 0.51 82.42 133 0.52 65.32 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>7</th> <th>2066</th> <th></th>									7	2066	
$ \begin{bmatrix} 2063 & 10 & \frac{8212}{11} & \frac{199}{128} & \frac{1111}{11} & \frac{255}{105} & \frac{173}{230} & \frac{776}{120} & \frac{177}{120} & \frac{8512}{120} & \frac{196}{128} & \frac{133}{130} & \frac{8386}{130} & \frac{133}{120} \\ 2070 & 11 & \frac{8161}{12} & \frac{173}{12} & \frac{115}{12} & \frac{10515}{102} & \frac{230}{148} & \frac{148}{7471} & \frac{777}{11} & \frac{163}{105} & \frac{105}{7859} & \frac{172}{10} & \frac{10}{8204} & \frac{179}{179} \\ 2072 & 13 & \frac{7254}{14} & \frac{142}{124} & 081 & \frac{9109}{100} & 178 & 102 & \frac{6838}{110} & \frac{137}{10} & \frac{078}{77} & \frac{775}{15} & \frac{143}{14} & 0.76 & \frac{775}{7628} & \frac{149}{14} \\ 2074 & 15 & \frac{6513}{15} & \frac{199}{19} & 0.60 & \frac{8634}{854} & \frac{149}{149} & 0.74 & \frac{6796}{6796} & \frac{117}{17} & 0.59 & \frac{7705}{122} & \frac{110}{14} & \frac{0.61}{7628} & \frac{773}{122} & \frac{110}{16} & \frac{0.61}{7628} & \frac{773}{122} & \frac{110}{122} & \frac{0.61}{7628} & \frac{772}{122} & \frac{110}{122} & \frac{0.61}{7628} & \frac{773}{122} & \frac{110}{14} & \frac{0.61}{14} & \frac{6534}{149} & \frac{0.74}{6796} & \frac{6532}{177} & \frac{100}{50} & \frac{0.61}{7528} & \frac{112}{122} & \frac{0.61}{7628} & \frac{772}{122} & \frac{111}{122} & \frac{0.61}{7628} & \frac{773}{122} & \frac{112}{122} & \frac{0.61}{122} & \frac{775}{122} & \frac{112}{122} & \frac{0.61}{11} & \frac{775}{122} & \frac{112}{122} & \frac{0.61}{122} & \frac{775}{122} & \frac{112}{122} & \frac{0.61}{11} & \frac{775}{122} & \frac{112}{122} & \frac{0.61}{122} & \frac{775}{122} & \frac{112}{122} & $									-		
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2071 12 7328 152 0.82 9977 2.04 124 72.07 149 0.91 78.01 161 0.98 8190 189 2072 13 72.54 142 0.81 9109 178 102 69.88 137 0.78 77.91 152 0.87 73.51 155 2073 14 72.18 1.33 0.71 90.53 1.66 0.88 68.11 1.25 0.67 77.59 143 0.76 75.28 1.40 2074 15 65.10 9 0.51 85.34 149 0.74 67.35 117 0.59 7105 1.22 0.61 75.28 1.40 2076 17 66.87 0.92 0.66 75.39 1.04 0.41 65.41 0.99 0.42 68.07 102 0.44 75.20 112 2077 18 66.78 0.92 0.66 75.39 0.74 0.40 6	2.55 1.73 76.80 1.77 1.20 85.12 1.96 1.33 83.86 1.93 1.31										
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2089 30 28.13 0.00 0.00 40.44 0.00 0.00 36.53 0.00 0.00 41.18 0.00 0.00 47.77 0.00 # of years 30 3	0.00 0.00 36.53 0.00 0.00 41.18 0.00 0.00 47.77 0.00 0.00	30.03	0.00	0.00	40.44	0.00] 0.00	28.13	30		# of upp
# of years 30 L-Moments 48 36 57 42 51 39 49 37 53	57 42 51 39 49 37 53 40		42	57		36	48				# or years
GEV w/Lmom lambda1 78.92 92.80 81.19 80.32 80.32 86.53		81.19		0.	92.80		.0	78.92			GEV w/Lmom
lambda2 17.57 20.43 20.54 18.65 19.12								17.57			
lambda3 5.81 3.35 7.58 6.62 9.36	758 6.62 9.36	7.58			3.35						
skew 0.33 0.16 0.37 0.35 0.49											

(Step 5 - 6 Example: Calculate ratios between baseline and future for each GCM for each grid*) Moakley Park, South Boston, MA

	2070s (2060-2089) RCP8.5 Grid1													
T-yr Event	Max of bcc- csm1-1.1	Max of bcc- csm1-1-m.1	Max of ccsm4.6	Max of cnrm- cm5.1	Max of csiro mk3-6-0.1	Max of gfdl- cm3.1	Max of giss- e2-h.6	Max of giss- e2-r.6	Max of hadgem2- ao.1	Max of hadgem2- cc.1	Max of inmcm4.1	Max of ipsl- cm5a-lr.1	Max of miroc5.1	Max of mri- cgcm3.1
						F	Ratios to mod	deled baselin	e					
2-yr, 24-hr	1.14	1.47	1.15	1.10	1.16	1.10	1.13	1.09	1.31	1.30	1.12	1.18	1.19	1.24
5-yr, 24-hr	1.15	1.51	1.30	1.16	1.20	1.05	1.24	1.10	1.32	1.27	1.18	1.29	1.22	1.25
10-yr, 24-hr	1.16	1.50	1.41	1.21	1.29	1.02	1.31	1.11	1.32	1.28	1.19	1.40	1.25	1.21
25-yr, 24-hr	1.17	1.45	1.55	1.30	1.49	0.99	1.39	1.13	1.32	1.32	1.18	1.61	1.30	1.15
50-yr, 24-hr	1.19	1.40	1.66	1.39	1.71	0.96	1.45	1.15	1.31	1.37	1.16	1.80	1.33	1.09
100-yr, 24-hr	1.20	1.34	1.78	1.48	1.99	0.94	1.51	1.17	1.30	1.43	1.13	2.03	1.36	1.03
200-yr, 24-hr	1.22	1.28	1.90	1.58	2.36	0.92	1.56	1.19	1.29	1.50	1.09	2.31	1.40	0.97
500-yr, 24-hr	1.25	1.19	2.08	1.74	3.01	0.89	1.63	1.22	1.27	1.61	1.04	2.75	1.45	0.89

Future design depth / baseline design depth = ratio

*This chart shows ratios for the 2070 planning horizon only.

2070s example for 10-yr, 24-hr:

5.267 in. / 4.557 in. = 1.16

(Step 7 Example: Calculating mean of the ratios for all GCMs and adding ratios to NOAA Atlas 14 Values*) Moakley Park, South Boston, MA

	2070s (2060-2089) RCP8.5 Grid1										
Return Period	NOAA 14 Precip. (in.)	NOAA 14 Precip. 5% Cl (in.)	NOAA 14 Precip. 95% CI (in.)	No. of Models	Mean of ratios	Std Dev. of ratios	5% CL of ratios	95% CL of ratios	Projected Precip. (in.)	Projected Precip. 5% CI (in.)	Projected Precip. 95% CI (in.)
2-yr	3.3	2.8	3.8	14	1.19	0.11	1.15	1.24	3.9	3.7	4.0
5-yr	4.3	3.6	5.1	14	1.23	0.11	1.18	1.28	5.3	5.1	5.5
10-yr	5.1	4.3	6.1	14	1.26	0.13	1.21	1.32	6.5	6.2	6.7
25-yr	6.3	5.1	8.0	14	1.31	0.18	1.23	1.39	8.2	7.8	8.7
50-yr	7.2	5.6	9.3	14	1.35	0.24	1.25	1.46	9.7	8.9	10.4
100-yr	8.1	6.1	11.0	14	1.41	0.33	1.26	1.55	11.4	10.2	12.6
200-yr	9.3	6.4	12.8	14	1.47	0.45	1.27	1.67	13.6	11.8	15.4
500-yr	11.1	7.3	15.9	14	1.57	0.65	1.29	1.86	17.5	14.3	20.6

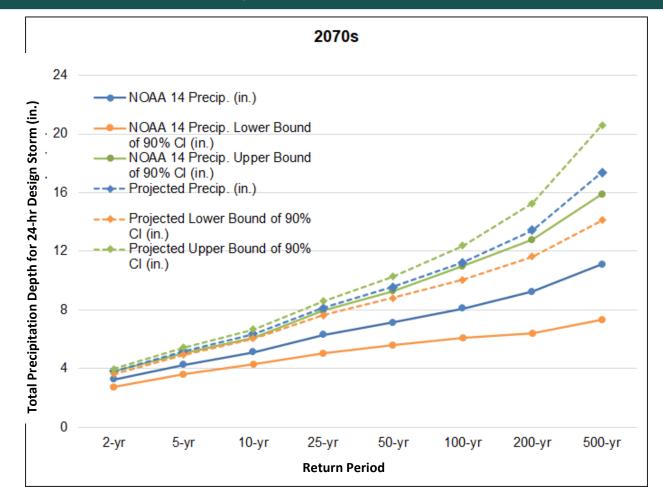
*This chart shows NOAA Atlas 14 values and projected total precipitation depths for 24-hr design storms for the 2070 planning horizon using an ensemble of 14 GCMs from LOCA dataset following NCHRP 15-61 methodology.

(Step 8 Example: Calculating mean of the projected 24-hour precipitation depths for all grids*) Moakley Park, South Boston, MA

	2070s (2060-2089) RCP8.5 Average of the Grids								
Return Period	Projected Precip. (in.)	Projected Precip. 5% CI (in.)	Projected Precip. 95% CI (in.)						
2-yr	3.8	3.6	4.0						
5-yr	5.2	4.9	5.4						
10-yr	6.4	6.1	6.7						
25-yr	8.1	7.6	8.6						
50-yr	9.5	8.8	10.3						
100-yr	11.2	10.1	12.4						
200-yr	13.5	11.6	15.3						
500-yr	17.4	14.1	20.6						

*This chart shows mean of the projected total precipitation depth for 24-hr design storms for the 2070 planning horizon using an ensemble of 14 GCMs from LOCA dataset following NCHRP 15-61 methodology.

(Step 9 Example: Comparing the projected precipitation quantiles with NOAA Atlas 14 historical estimates*) Moakley Park, South Boston, MA



*This figure shows comparison between projected precipitation quantiles with NOAA Atlas 14 historical estimates for the 2070s planning horizon only.

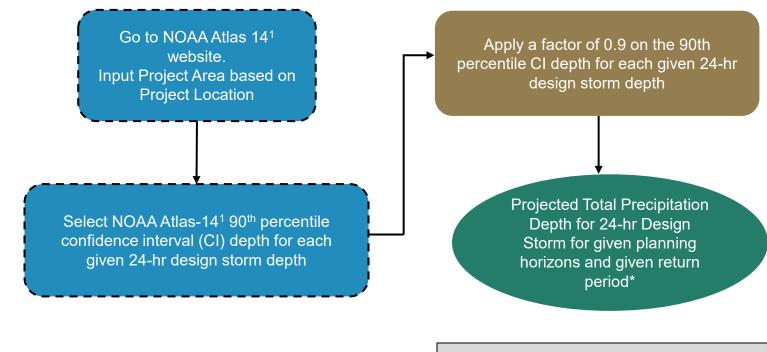
(Step 11 Example: 24-hr design storm hyetographs for peak intensity for given planning horizon and design storm*) Moakley Park, South Boston, MA

Return Period	NOAA Atlas 14 Present Baseline - 24hr (in)	Tier 3 Projected Total Precip Depth 2070 Values - 24hr (in)
2-yr	3.3	3.8
5-yr	4.3	5.2
10-yr	5.1	6.4
25-yr	6.3	8.1
50-yr	7.2	9.5
100-yr	8.1	11.2
200-yr	9.3	13.5
500-yr	11.1	17.4

*This chart shows mean of the projected total precipitation depth for 24-hr design storms for the 2070 planning horizon using an ensemble of 14 GCMs from LOCA dataset following NCHRP 15-61 methodology.

Tiered Methodology to Assess Projected Total Precipitation Depth for 24-hr Design Storm Tier 1 Projects*

Given Standards Output from Tool: Planning Horizon (2030, 2050, 2070); Return Period (5-yr, 10-yr, 25-yr, 50-yr, 100-yr, 200-yr, 500-yr)



* Tier 1 Projects will also receive output from the Tool and an Attention note to compare the calculated depth using the methodology shown in this figure with the Tool output.

1. NOAA Atlas 14 Precipitation Frequency Estimates: Northeastern States; NOAA Atlas 14, Volume 10, Version 3

Legends	
Data Gathering	
Calculation steps	
Design Criteria	\bigcirc
Existing practice	(2222)

Tiered Methodology to Assess Projected Total Precipitation Depth for 24-hr Design Storm Tier 1 Projects (24-hr design storm depths for recommended return periods) Moakley Park, South Boston, MA

Return Period	NOAA Atlas 14 Present Baseline - 24hr (in)	NOAA Atlas 14 Present Baseline - 24hr (90th percentile) (in)	Tier 1 90% of 90th percentile of NOAA baseline (in)
2-yr	3.3	3.8	3.4
5-yr	4.3	5.1	4.6
10-yr	5.1	6.1	5.5
25-yr	6.3	8.0	7.2
50-yr	7.2	9.3	8.4
100-yr	8.1	11.0	9.9
200-yr	9.3	12.8	11.5
500-yr	11.1	15.9	14.3

CLIMATE RESILIENCE DESIGN STANDARDS

PROJECTED PEAK INTENSITY DESIGN CRITERIA METHODS

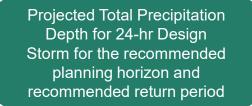
All Tiers

Version 1.4 DECEMBER 2024



Tiered Method to Assess Projected Peak Intensity for All Tiers

Given Standards Output from Tool: Projected Total Precipitation Depth for 24-Hr Design Storm for recommended Planning Horizon (2030, 2050, 2070); Return Period (5-yr, 10-yr, 25-yr, 50-yr, 100-yr, 200-yr, 500-yr)



Use NOAA Atlas14²/NRCS Type C and D³/SCS Type III⁴ Distribution to estimate hourly/sub-hourly peak intensities

Projected Design storm hyetograph and peak intensity for given 24-hr design storm depths

Legends	
Calculation steps	
Design Criteria	\bigcirc
Existing practice	יבבבו

- 1. NOAA Atlas 14 Precipitation Frequency Estimates: Northeastern States; NOAA Atlas 14, Volume 10, Version 3
- Engineering Field Handbook Chapter 2: Estimating Runoff and Peak Discharges: Massachusetts EFH-2 Supplement Number: MA-EFH2. <u>https://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/stelprdb10971</u> 25.pdf
- 3. HEC-HMS Technical Reference Manual SCS Storm; https://www.hec.usace.army.mil/confluence/hmsdocs/hmstrm/precipitat ion/scs-storm

Tiered Methodology to Assess Projected Peak Intensity

Example: 24-hr design storm hyetographs for projected peak intensity for given planning horizon and design storm*, Moakley Park, South Boston, MA using SCS Type III Distribution

Return Period	NOAA Atlas 14 Present Baseline - 24hr (in)	Projected Total Precip Depth 2070 Values - 24hr (in)
2-yr	3.3	3.8
5-yr	4.3	5.2
10-yr	5.1	6.4
25-yr	6.3	8.1
50-yr	7.2	9.5
100-yr	8.1	11.2
200-yr	9.3	13.5
500-yr	11.1	17.4

*These charts show 24-hr design storm hyetographs for peak intensity for the 2070s planning horizon only

10yr - 24 hr 2070s		6.4 in	
Duration (hr)	Ratio	Cumulative depth (in.)	Hourly peak intensity (in./hr)
0	0	0	0
1	0.01	0.06	0.06
2	0.02	0.13	0.06
3	0.03	0.19	0.07
4	0.04	0.27	0.08
5	0.06	0.36	0.09
6	0.07	0.45	0.10
7	0.09	0.57	0.12
8	0.11	0.72	0.15
9	0.15	0.92	0.20
10	0.19	1.19	0.27
11	0.25	1.58	0.38
12	0.50	3.15	1.58
13	0.75	4.73	1.58
14	0.81	5.11	0.38
15	0.85	5.38	0.27
16	0.89	5.58	0.20
17	0.91	5.73	0.15
18	0.93	5.85	0.12
19	0.94	5.94	0.10
20	0.96	6.03	0.09
21	0.97	6.11	0.08
22	0.98	6.18	0.07
23	0.99	6.24	0.06
24	1	6.30	0.06

CLIMATE RESILIENCE DESIGN STANDARDS

PROJECTED RIVERINE DESIGN CRITERIA TIERED METHODS

Tier 3 & 2 Projects – Page 2

Tier 1 Projects – Page 3

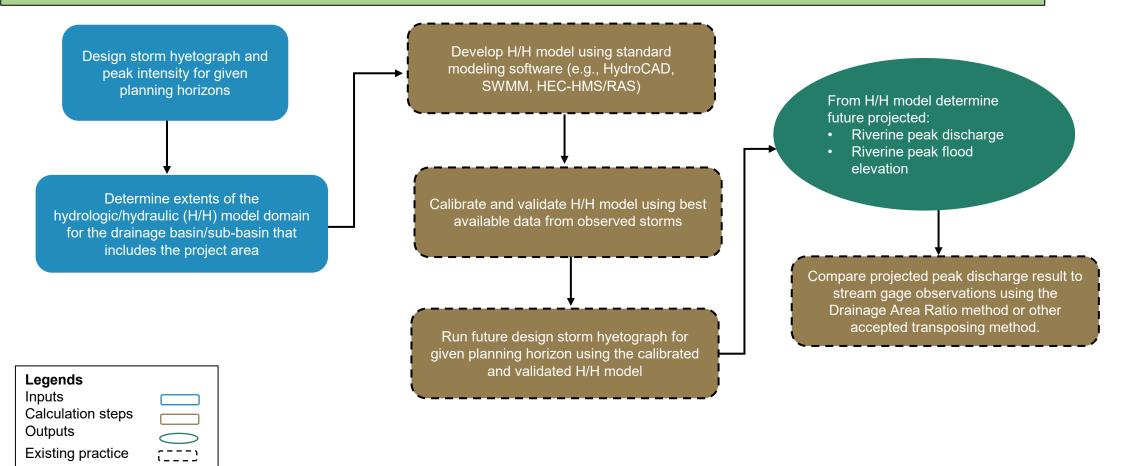
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DECEMBER 2024



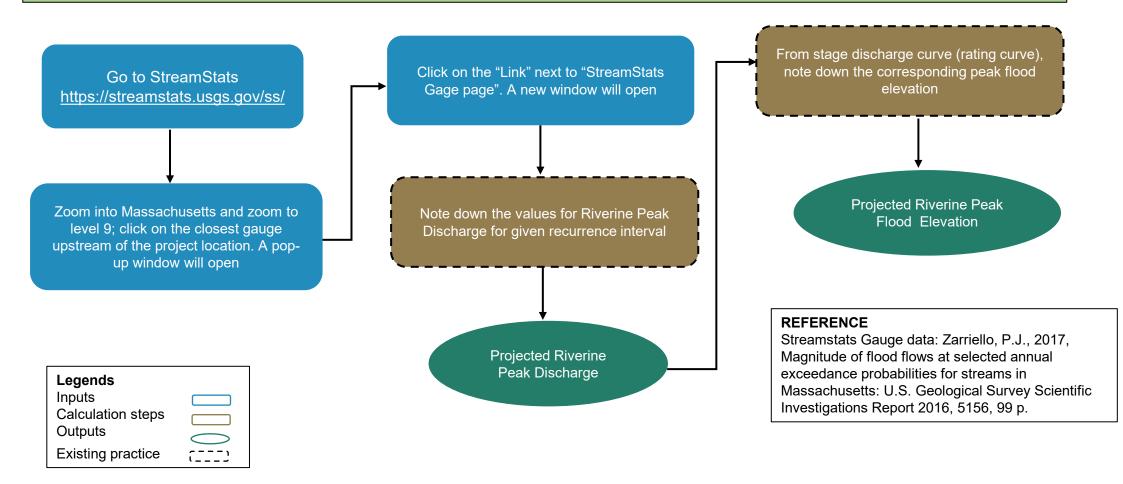
Tiered Method to Assess Projected Riverine Peak Discharge Criteria For Tier 3/Tier 2 Projects

Given Standards Output from Tool: Projected 24-hour Design Storm for Recommended Planning Horizon (2030, 2050, 2070); Recurrence Interval (5-yr, 10-yr, 25-yr, 50-yr, 100-yr, 200-yr, 500-yr)



Tiered Method to Assess Projected Riverine Peak Discharge Criteria For Tier 1 Projects

Given Standards Output from Tool: Projected 24-hour Design Storm for Recommended Planning Horizon (2030, 2050, 2070); Recurrence Interval (5-yr, 10-yr, 25-yr, 50-yr, 100-yr, 200-yr, 500-yr)



CLIMATE RESILIENCE DESIGN STANDARDS

PROJECTED HEAT INDEX DESIGN CRITERIA TIERED METHODS

Tier 3 Projects – Pages 2-9

Tier 2 & 1 Projects – Page 10

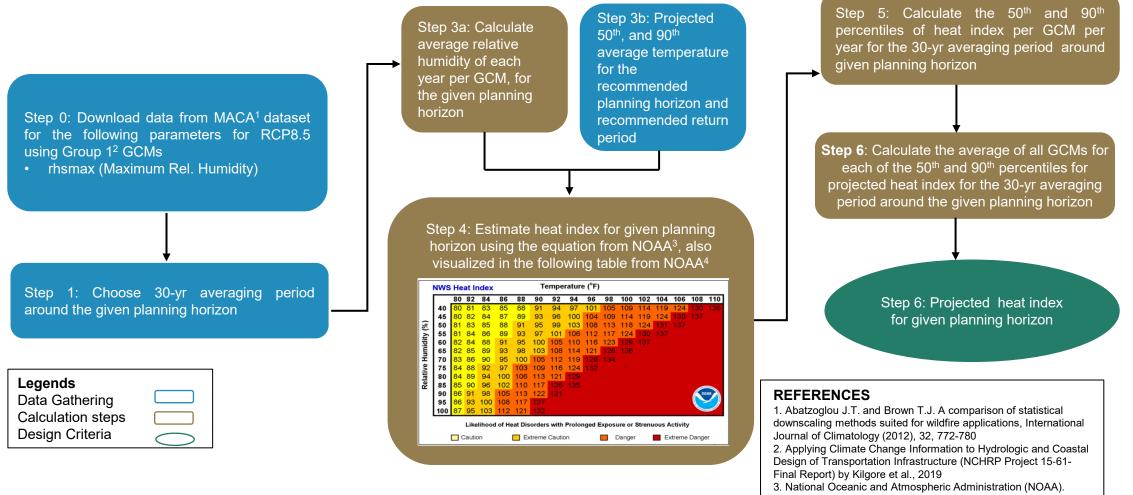
Version 1.4

DECEMBER 2024



Tiered Method to Assess Projected Heat Index Tier 3 Projects (Highest Level of Effort)

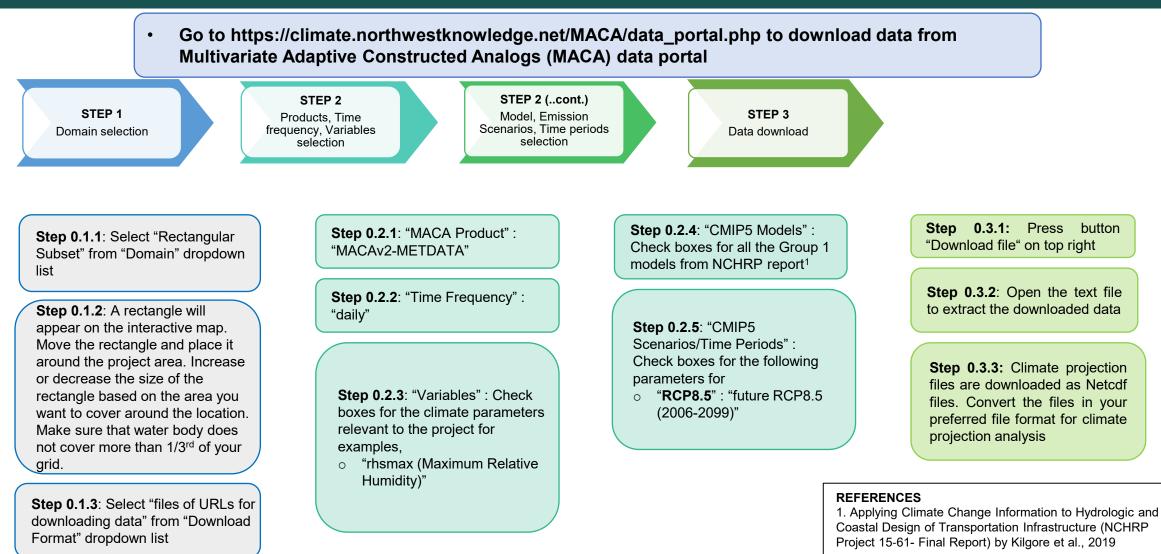
Given from Standards Output: Average Temperature for recommended Planning Horizon (2030, 2050, 2070); Percentile (50th, 90th)



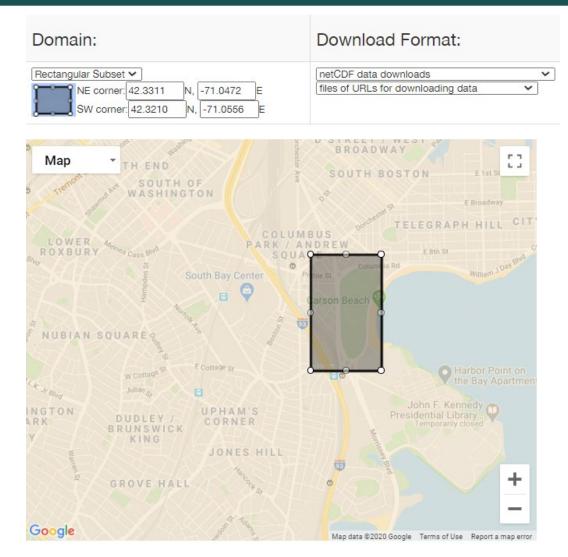
2014. The Heat Index Equation.

https://www.wpc.ncep.noaa.gov/html/heatindex_equation.shtml 4. National Oceanic and Atmospheric Administration (NOAA).n.d. Heat Index. https://www.weather.gov/safety/heat-index

Tiered Method to Assess Projected Heat Index - Tier 3 Projects (Step 0: Complete MACA data download)



Download MACA Dataset (Example: Project Area, and Download Format Selection)



Download MACA Dataset (Example: Product, Time Frequency, and Variables Selection)

MACA PRODUCT

MACAv2-LIVNEH
 MACAv1-METDATA
 MACAv2-METDATA

TIME FREQUENCY

🖲 daily

O monthly

O Annual

O DJF(Dec-Feb)

O MAM (March-May)

O JJA (June-Aug)

○ SON (Sept-Nov)

VARIABLES



huss (Specific Humidity)
 pr (Precipitation)
 rhsmax (Maximum Relative Humidity)
 rhsmin (Minimum Relative Humidity)
 rsds (Downwelling Solar Radiation)
 tasmin(Minimum Air Temperature)
 tasmax(Maximum Air Temperature)
 vpd (Vapor Pressure Deficit)
 uas (Eastward Wind Component)
 vas (Northward Wind Component)

Download MACA Dataset (Example: Group1¹ GCM Selections)

CMIP5 MODELS

Select All DeSelect All bcc-csm1-1 (China) bcc-csm1-1-m (China) BNU-ESM (China) CanESM2 (Canada) CCSM4 (USA) CNRM-CM5 (France) CSIRO-Mk3-6-0 (Australia) GFDL-ESM2G (USA) GFDL-ESM2M (USA) HadGEM2-CC365 (United Kingdom) HadGEM2-ES365 (United Kingdom) inmcm4 (Russia) IPSL-CM5A-LR (France) IPSL-CM5A-MR (France) IPSL-CM5B-LR (France) MIROC5 (Japan) MIROC-ESM (Japan) MIROC-ESM-CHEM (Japan) MRI-CGCM3 (Japan) NorESM1-M (Norway)

REFERENCES

1. Applying Climate Change Information to Hydrologic and Coastal Design of Transportation Infrastructure (NCHRP Project 15-61- Final Report) by Kilgore et al., 2019

Download MACA Dataset (Example: Emission Scenario (RCP8.5) and Time Selection)

RCP 8.5 cp85 (2006-2010) cp85 (2011-2015) cp85 (2016-2020) cp85 (2021-2025) cp85 (2026-2030) cp85 (2031-2035) cp85 (2036-2040) cp85 (2041-2045) cp85 (2046-2050) cp85 (2051-2055) cp85 (2056-2060) cp85 (2061-2065) cp85 (2066-2070) cp85 (2071-2075) cp85 (2076-2080) cp85 (2081-2085) cp85 (2086-2090) cp85 (2091-2095) cp85 (2096-2099) future RCP8.5 (2006-2099) Gifuture RCP8.5 (2006 2099

Tiered Method to Assess Projected Heat Index - Tier 3 Projects (Step 3 Example: Calculate the median max. temp. and median avg. rel. Humidity*) Moakley Park, South Boston, MA

	2070s Tasmax																						
	Max of bcc-	Max of bcc-	Max of	Max of CNRM	Max of	Max of	Max of	Max of IPSL-	Max of IPSL	Max of	Max of MRI-	Median Max											
Row Labels	csm1-1	csm1-1-m	CCSM4		CSIRO-Mk3-6-	HadGEM2-	inmcm4	CM5A-LR	CM5B-LR	MIROC5	CGCM3	of Max-											
					0	CC365						Temp											
2060	104.5	99.3	99.9	97.1	102.1	105.7	97.7	98.2	100.4	101.0	97.6	99.87											
2061 2062	96.4 92.2	102.4 101.5	102.0 103.0	99.1 104.8	102.0 101.0	105.0 109.2	99.3 96.7	101.0 99.3	101.6 100.4	101.3 97.0	105.2 97.0	101.64 100.43											
2062	101.4	101.5	105.0	104.8	101.0	109.2	96.7	100.7	99.1	97.0	102.0	100.45											
2003	101.4	103.2	100.8	103.8	101.8	105.5	97.9	100.7	96.7	102.7	96.7	101.41	1	1				1					
2065	98.0	102.3	101.2	96.8	107.9	100.5	92.6	102.0	98.8	101.1	96.9		Average of	Average	Average	Average	Average of	Average	Average	Average	Average	Average	RHavg
2066	100.6	101.4	98.7	94.5	104.9	103.5	99.7	102.6	103.3	99.6	97.6	YEAR	bcc-csm1-1	of bcc-	of CNRM-	of CSIRO-	HadGEM2-	of	of IPSL-	of IPSL-	of		MEDIAN OF
2067	99.4	101.6	101.9	96.9	107.8	102.9	96.7	97.6	101.8	100.0	98.2	-		csm1-1-m	CM5	Mk3-6-0	CC365	inmcm4	CM5A-LR	CM5B-LR	MIROC5	CGCM3	ALL GCMS
2068	100.0	101.8	99.2	101.7	105.1	109.6	97.2	105.0	99.1	100.7	98.3	2060	78.5	79.2	79.4	78.7	76.7	78.9	79.4	74.6	79.1	79.2	79.0
2069	103.3	102.0	100.0	104.7	102.1	101.2	102.0	101.9	100.0	101.4	96.7	2061	79.5	78.6	79.2	81.2	75.9	80.3	76.7	77.7	76.9	77.8	78.2
2070	101.9	101.8	104.2	103.6	101.1	107.7	94.8	104.2	100.5	98.5	105.2	2062	79.5	79.4	79.2	80.1	76.5	80.6	76.6	77.2	78.9	79.4	79.3
2071	102.8	103.3	100.5	105.3	98.7	108.1	95.2	99.2	100.6	104.1	100.9	2063	79.6	80.1	76.8	79.6	75.1	78.2	77.2	77.2	77.8	79.6	78.0
2072	94.1	108.0	103.1	97.2	103.7	104.7	93.8	100.6	103.2	103.4	98.1	2064	76.8	77.7	78.6	79.1	76.0	79.5	76.0	77.8	77.6	79.2	77.7
2073	105.8	100.8	104.5	103.4	103.1	111.8	92.5	102.6	101.0	102.6	98.1	2065	79.4	78.0	78.7	77.6	74.1	79.4	76.2	77.7	75.9	78.9	77.8
2074	102.3	98.9	104.4	99.5	107.7	107.6	99.6	100.1	104.0	100.0	104.6	2066	79.6	79.6	80.3	79.9	74.6	79.9	76.6	77.3	78.9	78.5	79.3
2075	102.5	101.0	104.7	102.4	106.1	109.6	93.3	102.9	97.7	101.5	98.2	2067	79.5	78.3	79.3	78.3	76.5	80.2	75.6	78.6	78.0	78.6	78.4
2076	102.0	101.2	102.7	103.2	101.9	106.4	93.1	99.1	102.6	100.8	98.5	2068	79.1	80.4	78.3	76.7	75.8	80.9	76.9	75.6	79.3	79.2	78.7
2077	102.4	95.1	98.7	97.1	103.0	113.4	103.4	105.9	100.2	102.1	98.1	2069	78.3	77.7	80.2	77.6	76.4	79.7	75.7	76.1	77.1	77.8	77.6
2078	105.3	99.8	102.1	107.8	104.6	108.3	95.4	105.8	100.1	101.9	98.7	2070	79.0	78.4	77.9	78.0	76.5	79.1	74.6	77.6	78.3	80.2	78.1
2079 2080	101.2 104.1	102.5 100.9	102.2 103.6	98.9 102.3	98.3 104.8	105.7 109.1	98.6 97.4	103.2 104.5	102.3 102.6	105.2 103.0	97.7 98.6	2071	78.6	79.3	76.9	82.2	74.6	79.1	77.1	75.5	77.1	79.7	77.8
2080	104.1	100.9	105.6	102.5	104.8	109.1	97.4	104.5	102.0	98.7	96.3	2072	79.1	77.8	78.0	78.2	78.1	79.7	75.0	76.5	77.1	80.0	78.0
2081	104.5	104.5	104.9	103.2	104.8	112.8	95.9	104.2	100.1	101.5	100.9	2073	77.4	78.2	77.6	78.9	76.6	79.5	74.7	75.9	77.3	76.4	77.3
2083	100.3	97.9	102.1	98.8	104.4	112.0	95.5	103.1	102.5	101.5	100.0	2074	80.0	80.9	80.3	76.9	74.4	80.1	76.7	76.5	76.9	79.5	78.2
2084	101.5	103.4	103.2	97.3	102.1	104.6	99.9	105.0	102.5	98.2	97.8	2075	78.8	80.2	79.3	78.8	74.7	78.7	77.1	75.8	77.9	78.3	78.5
2085	102.6	101.6	104.9	98.5	100.9	112.9	93.9	109.2	101.3	102.4	96.9	2076	79.5	79.4	77.2	79.7	75.0	79.5	76.3	77.1	77.2	78.7	78.0
2086	105.1	104.8	107.2	97.1	104.8	112.5	98.7	105.8	102.3	99.7	102.2	2077	77.5	79.7	78.0	79.1	75.5	80.3	75.9	75.4	79.8	78.9	78.5
2087	96.9	104.0	107.2	96.8	104.8	109.7	102.6	105.8	102.3	105.1	97.4	2078	79.2	81.1	77.3	79.1	75.7	80.2	75.5	76.0	77.8	80.0	78.5
2088	102.4	102.8	105.3	101.3	103.6	111.6	99.4	106.4	102.0	100.7	100.6	2079	78.9	77.8	79.4	81.2	76.4	80.1	77.7	76.1	77.1	78.0	77.9
2089	108.0	105.0	107.5	101.8	110.3	105.1	91.9	105.6	107.5	105.5	101.7	2080	77.4	80.8	77.6	81.7	73.5	77.6	75.9	77.1	76.5	78.1	77.5
	1	1		ł	ł – – ł				I	· · · · · ·		2081	77.9	78.8	78.3	78.6	74.2	79.6	73.9	74.8	76.5	79.4	78.1
				*	These cha	irts show o	calcula	tions fo	r the 207	70 plar	nning 🎼	2082	79.3	78.6	76.9	80.3	75.5	80.0	78.6	75.3	76.7	80.7	78.6
									20/	- 5 p.u	e	2083	78.7	79.5	79.0	79.9	74.3	79.2	74.4	76.0	79.1	79.0	79.0
				h	orizon on	ly						2084	77.4	80.5	78.3	79.6	76.3	79.9	76.3	74.8	79.2	79.1	78.7
												2085	79.8	79.1	77.2	81.9	75.8	79.1	73.9	78.0	76.2	80.1	78.5
												2086	78.9	77.8	80.2	79.3	74.0	78.6	73.9	78.7	76.5	79.1	78.7
-												2087	80.7	80.1	78.4	80.5	75.2	81.5	76.2	78.6	78.5	78.5	78.6
V	'ERSION	N 1.4 M	ETH(DDS								2088	80.3	80.3	77.9	78.4	75.8	79.4	74.9	76.0	78.7	R <u>∕</u>178.4	78.4
г	acamb	or 202/	1									2089	77.4	79.5	77.7	78.9	75.1	79.2	75.1	78.8	77.1	78.1	77.9

December 2024

Tiered Method to Assess Projected Heat Index - Tier 3 Projects (Step 4: Calculate heat index per year based on the NOAA Heat Index Eqn.)* Example: Moakley Park, Boston

HI = -42.379 + 2.04901523*T + 10.14333127*RH -.22475541*T*RH - .00683783*T*T - .05481717*RH*RH + .00122874*T*T*RH + .00085282*T*RH*RH -.00000199*T*T*RH*RH

where,

HI = *Heat Index*

T = *Temperature* (*tasmax*)

RI = *Relative Humidity (average rhsmax)*

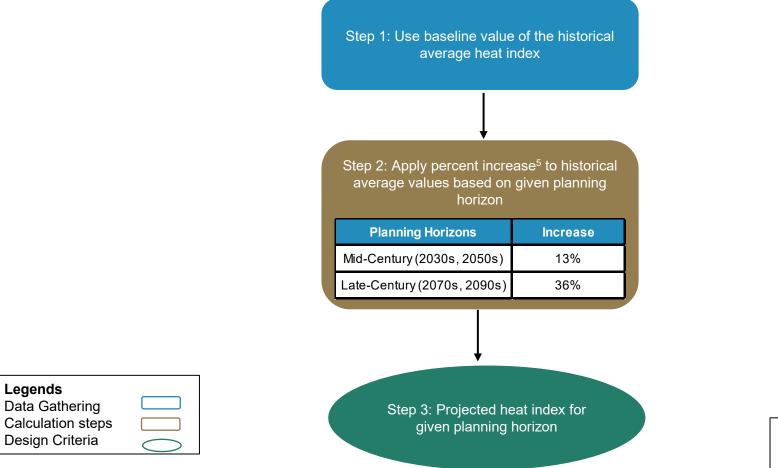
2070s Data									
Year	RHavg Median of Median Max of All GCMs Max-Temp Eqn								
2060	79	100	156						
2061	78	102	164						
2062	79	100	159						
2063	78	101	162						
2064	78	102	166						
2065	78	101	160						
2066	79	101	160						
2067	78	100	158						
2068	79	101	160						
2069	78	102	164						
2070	78	102	165						

10th percentile	78	100	158
50th percentile	78	102	166
90th percentile	79	104	177

*This chart shows calculations for the 2070 planning horizon only

Tiered Method to Assess Projected Heat Index Tier 2 and Tier 1 Projects

Given from Standards Output: Average Temperature for recommended Planning Horizon (2030, 2050, 2070); Percentile (50th, 90th)



REFERENCES

5. Percent Increase data based on Climate Change Vulnerability Assessment (November 2015) report for City of Cambridge, MA (Table 2, pp. 23)