

Eastern Hampshire District Court Belchertown, MA

HVAC SYSTEM EVALUATIONS COVID-19

Office of Court Management

December 28, 2021

Tighe&Bond

100% Recyclable

Section 1 Existing Conditions & Site Observations

Tighe & Bond visited the Eastern Hampshire District Court in Belchertown, MA on February 24, 2021. While on site we inspected the rooftop air handling equipment and toured the facility to determine if the spaces generally matched usages noted on the architectural plans.

Site Visit Attendees:

- Office of Court Management:
 - Alfred Benoit, Court Facilities Staff
- Tighe & Bond
 - Todd Holland, PE, Senior Mechanical Engineer
 - Matt Mancini, Staff Mechanical Engineer

1.1 Existing Ventilation System

The Eastern Hampshire District Court is a leased building that was constructed in 2006, is a single story on a slab, and is approximately 30,000 square feet in size. There have been no significant changes or additions to the building or its systems since construction.

Ventilation air is provided by eight constant-volume, single-zone packaged rooftop units. Each unit consists of a mixing box with 100% outdoor air economizer, 2" MERV-13 filters, constant-speed supply fan, direct-expansion (DX) cooling coil, gas-fired furnace, refrigeration compressor(s) and condenser. There are no return or exhaust fans in the air handlers, just barometric relief dampers for when the units are in economizer mode. Supply air is distributed through metal ductwork with ceiling-mounted diffusers and return grilles.

The toilet rooms that serve the public and jury deliberation rooms are served by roofmounted exhaust fans. Small toilet rooms are served by individual ceiling-mounted exhaust fans.

The mechanical plans we reviewed do not show a separate exhaust fan serving the holding cells, they show return air ducted back to the rooftop unit. However, there is a rooftop exhaust fan located above the area, which most likely serves the holding cells. It was not operating at the time of our visit, and the exhaust grilles in the holding cells were not active, although dust on the grill faces indicates they are or may have been active. The snow melt pattern around this fan also indicates that it runs, see Photo 2 and the explanation that follows.

A small split-system serves the tel/data room. Electric-resistance wall heaters serve vestibules and the public toilet rooms.



Photo 1 – Representative Rooftop Air Handlers



Photo 2 – Representative Exhaust Fans

The exhaust fan in the background, upper left corner of Photo 2, serves the toilet rooms in the Jury Deliberation area, and was running at the time of our site visit. We suspect that the unit in the foreground serves the holding cells. We observed that it was not running, but the snow melt pattern indicates that it has run recently.

All HVAC units are from the original construction and appear to be in fair condition, although at or near the end of their expected service lives. There are comfort issues throughout the building that were noted by staff, which we feel may be due to the limited zoning of the rooftop units, and the coarse staging of cooling and heating (which is largely just on or off).

Table 1 summarizes the rooftop units' designed airflow rates, the MERV rating of the installed filters, and the observed condition.

Existing Air H	Handling Units			
Unit	Original Design Airflow (CFM)	Original Design Min. O.A. (CFM)	Pre/Final Filters	Condition
RTU-1	3,400	Unknown	2" MERV-13	Fair
RTU-2	5,000	Unknown	2" MERV-13	Fair
RTU-3	4,000	Unknown	2" MERV-13	Fair
RTU-4	3,000	Unknown	2" MERV-13	Fair
RTU-5	3,400	Unknown	2" MERV-13	Fair
RTU-6	2,400	Unknown	2" MERV-13	Fair
RTU-7	5,000	Unknown	2" MERV-13	Fair
RTU-8	5,000	Unknown	2" MERV-13	Fair

TABLE 1

The filters in these units were recently upgraded to MERV-13 by an outside contractor.

1.2 Existing Control System

Rooftop units are controlled by programmable thermostats with 7-day schedules. All units were set to run the fan in "auto" mode, which runs the supply fan only when the unit is actively heating or cooling. This may have changed recently when new filters were installed. Units that serve the office areas are controlled by a central thermostat and four remote temperature averaging sensors. Units that serve the courtrooms and lockup areas are controlled by individual thermostats (single location used for heating or cooling call).

We noted that the thermostat that controls the lockup area is located in the guard office, which has a substantial amount of heat-generating electronics. According to staff the holding cells are often cold, and the temperature must be adjusted manually.



Photo 3 – Representative Thermostat

The exhaust fans serving the toilet rooms in the main lobby and jury deliberation areas are served by roof-mounted controlled by 24-hour timeclocks. The grilles in the main lobby toilet rooms were observed to be operating at the time of the visit. We suspect that the exhaust fan above the holding cells is also controlled by a 24-hour timeclock, which is not adjusted properly due to power failures.

The ceiling-mounted exhaust fans that serve small toilet rooms are controlled by occupancy sensors that also control the lighting.

Section 2 Recommendations

Below is a list of recommendations that we propose for the Eastern Hampshire District Court. Please refer to the "Master Recommendation List" for further explanation and requirements of the stated recommendations.

2.1 Filtration Efficiency Recommendations

We recommend the following measures be implemented for the existing air handling units that serve occupied areas:

RF-1: *Replace filters.*

We recommend the continued use of MERV-13 filters which meet the ASHRAE recommendation. Existing filters should be checked in March and April to ensure they are within their service lives and installed properly. The filter racks should be inspected to ensure that filters fit tightly and that end spacers are in place to minimize filter bypass.

RF-3: Install differential pressure sensors across the filter banks.

RF-3a: Connect the pressure sensor to a local alarm.

Maximum differential pressure should be set per manufacturer's recommendation based on air velocity to ensure filters are within their service lives. Typically this is not more than 1.0'' w.g.

2.2 Testing & Balancing Recommendations

The air handling units are approximately 15 years old and have not been tested and balanced since construction.

We recommend the following testing and balancing measures be implemented:

RTB-1: Test and balance air handling unit supply air and minimum outside air flow rates.

We recommend testing and balancing the outdoor air flow rates for all air handling units to the recommended minimum O.A. rates listed in Table 2.

Unit	Original Supply Airflow (CFM)	Original Design Min. O.A. (CFM)	Current Code Min. O.A. Requirements (CFM)	Recommended Minimum O.A. (CFM)
RTU-1	3,400	Unknown	404	600
RTU-2	5,000	Unknown	782	1,250
RTU-3	4,000	Unknown	520	520
RTU-4	3,000	Unknown	373	373
RTU-5	3,400	Unknown	563	680
RTU-6	2,400	Unknown	268	420
RTU-7	5,000	Unknown	1,102	1,250
RTU-8	5,000	Unknown	1,105	1,250

TABLE 2

Recommended Air Handler O.A. Flow Rates

Note: Although the ASHRAE Position Document on Infectious Aerosols recommends using the latest published standards and codes as a baseline for minimum ventilation, the mechanical code in effect at the time the HVAC systems were designed and constructed is what governs the required outdoor air flowrate for the HVAC equipment, if there have been no additions, renovations, alterations or changes in occupancy to the building. The 2015 International Mechanical Code does not prevent the continued use of existing systems.

Our ventilation air analysis discovered a few spaces that would not be able to receive the correct quantity of outdoor air based on today's code requirements at full occupancy. Our calculations showed that the additional outdoor air required would exceed the capacity of the gas furnaces. We recommend temporarily reducing the occupancy of the spaces that are not receiving the code required ventilation air. Table 3 lists the spaces that would require a reduced occupancy. The recommended outdoor air flow rates listed in Table 2 reflect the outdoor air requirements based on the reduced occupancy shown in Table 3.

Section 2 Recommendations

TABLE 3

	2015 IMC	Recommended
	Default Occupancy	Occupancy
Room & Associated AHU	(# of People)	(# of People)
<u>RTU-1</u>		
Conference Room 173	9	4
Conference Room 165	8	4
<u>RTU-3</u>		
Conference Room 105	7	2
<u>RTU-4</u>		
Staff Lounge	19	10
<u>RTU-5</u>		
Prisoner Visit 143	3	1
Attorney 144	3	2
<u>RTU-6</u>		
Conference Meeting 162	4	2
Conference Room 160	8	5
<u>RTU-7</u>		
Courtroom 1	139	120
Jury Deliberation 182	15	12
Conference 189	8	5
Conference 191	8	5
<u>RTU-8</u>		
Courtroom 2	139	120
Jury Deliberation 182	15	12
Conference 189	8	5
Conference 191	8	5

Our recommendations on outdoor airflows depend on each unit's specified heating capacity (low, medium, or high) and whether they serve perimeter zones with a higher heat load. The design documents do not specify a minimum outdoor air damper position for the units, and we were unable to determine the settings by visual inspection.

RTU-3 and RTU-4, which serve office areas on the west side of the building, were specified with low-capacity gas heat. Our recommendation is to set the outdoor air dampers at the code minimum, about 12.5% open.

RTU-1 and RTU-6, which serve office areas on the east side, and RTU-5 which serves the lockup area, were specified with medium-capacity gas heat. Our recommendation is to set

the outdoor air dampers at approximately 20% open, which should enable the units to maintain a 95°F discharge temperature in peak winter conditions.

RTU-2, RTU-7, and RTU-8 were specified with high-capacity gas heat. These units are on the upper roof and serve interior spaces that include the courtrooms, jury rooms, and main lobby. Our recommendation is to set the outdoor air dampers at 25% open, which we believe is about the maximum where the units will be able to provide discharge air conditions similar to original design under peak outdoor air conditions, assuming the coils are clean and their performance has not degraded over time.

The average airflow rate per person is shown below in Table 3. These values are based on the original full design supply airflow rate and the recommended outdoor airflow rates shown in Table 2. The airflow rate per person assumes a diversity factor of 70%, meaning the maximum number of occupants assumed to be in all zones at all times equates to 70% of the code default occupancy.

TABLE 3 Average Airflow Rate per Person								
	All Spaces	Courtrooms	Non- Courtroom Spaces					
Total Occupancy (People)	399	195	204					
Total Supply Air (CFM/Person)	78	39	116					
Outdoor Air (CFM/Person)	16	10	22					

The airflow rate per person for each Courtroom and Jury Room is shown below in Table 4. These values are based on full occupancy without taking diversity into account, the original full design supply airflow rate, and the recommended outdoor airflow rate.

TABLE 4

Airflow Rate per Person (Full Occupancy)

		Тс	otal Air	Out	door Air
Courtroom	Total People	Supply Airflow (CFM)	Airflow Rate (CFM/Person)	Outside Airflow (CFM)	Airflow Rate (CFM/Person)
Jury Deliberation 181	15	400	27	100	7
Jury Deliberation 182	15	400	27	100	7
Jury Pool 187	32	1,100	34	275	9
Courtroom 1	139	3,800	27	950	7
Courtroom 2	139	3,740	27	935	7

Note: Courtroom occupant density is based on 70 people/1,000 square feet, per the 2015 International Mechanical Code

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The airflow rate per person for each Courtroom and the Jury Pool Room, based on the reduced occupancy schedule provided by the Office of Court Management, is shown below in Table 4a.

		Τα	otal Air	Outdoor Air			
Courtroom	Total People	Supply Airflow (CFM)	Airflow Rate (CFM/Person)	Outside Airflow (CFM)	Airflow Rate (CFM/Person)		
Jury Deliberation 181	6	400	67	100	17		
Jury Deliberation 182	6	400	67	100	17		
Jury Pool 187	12	1,100	92	275	23		
Courtroom 1	24	3,800	158	950	40		
Courtroom 2	24	3,740	156	935	39		

TABLE 4a

Note: If occupancy is further reduced, the airflow rate per person will increase, assuming full airflow is being delivered to the space.

RTB-5: Test and balance all air inlets and outlets.

If specific areas within the Courthouse experience regular cooling and heating comfort complaints this may be an indication of a lack of airflow to the space. We recommend testing and balancing the air inlets and outlets serving those spaces to the designed values.

2.3 Equipment Maintenance & Upgrades

We recommend the following equipment maintenance and upgrades:

RE-2: Clean rooftop unit coils and drain pans.

While the cooling coils in the rooftop units may in generally good condition, they have operated for 16 years with only MERV-7 or MERV-8 filters for protection. These coils should be cleaned to maximize heat transfer and minimize pressure loss.

2.4 Control System Recommendations

We recommend the following for the control system:

RC-1: Implement a pre-occupancy flush sequence.

This sequence should start all rooftop units and exhaust fans before the building is occupied, with the start time calculated to provide three air changes per hour (ACH) of ventilation air, or for two hours before people arrive.

Note that this flush period should be run after a morning warmup period, if the units have this capability. During the morning warmup, units typically operate with the outdoor air damper fully closed to bring the space to occupied temperature. The flush period should be an extension of occupied mode, with units operating with outdoor air dampers open at or above minimum position.

RC-4: Confirm the economizer control sequence is operational.

2.5 Additional Filtration and Air Cleaning

We recommend the installation of the following air cleaning devices:

RFC-1: Install portable HEPA filters.

If the Eastern Hampshire District Court is to operate at a high capacity (i.e. 50% occupancy or greater), we recommend installing portable HEPA filters in high traffic areas, such as entrance lobbies or where people congregate outside courtrooms. They should also be considered for courtrooms, depending on the occupancy of the room and how much noise is generated from the filters. The noise levels will vary depending on the manufacturer.

2.6 Humidity Control

Installing duct mounted or portable humidifiers can help maintain the relative humidity levels recommended by ASHRAE. The feasibility of adding active humidification is determined by the building envelope. Buildings that were not designed to operate with active humidification can potentially be damaged due to a lack of a vapor barrier, adequate insulation, and air tightness.

Duct mounted humidifiers must be engineered, integrated into the building control system, tested, and commissioned. They are available in many configurations but require substantial maintenance and additional controls. They also run the risk of adversely affecting IAQ from growing microorganisms or leaking water through poorly sealed ductwork damaging insulation and ceilings. Portable humidifiers are easier to install and require less maintenance, but still have the potential to damage the building envelope.

While active humidification is not recommended as a whole building solution due to high installation costs, operational costs, potential to damage the building envelope and adversely affect poor IAQ, it may be warranted as a temporary solution in some areas.

2.7 Other Recommendations

2.7.1 Run Supply Fans Continuously During Occupied Hours

All units were set to run the fan in "auto" mode, which runs the supply fan only when the unit is actively heating or cooling. This should be changed on each of the systems to run the supply fans continuously in occupied mode, to supply ventilation air to the spaces. Note that this may cause comfort issues because supply air temperature can fluctuate as the heating and cooling is staged on and off, and the systems may not have been designed to operate like this originally.

2.7.2 Repair or Replace Controls for Exhaust Fans

We recommend repairing or replacing the controls for exhaust fans that were not working at the time of our visit. Exhaust fans can be interlocked the rooftop units that serve the surrounding space. Small toilet rooms with individual fans can continue using controls interlocked to the lights, but we recommend using a time delay relay that runs the fans for a period after the lights are switched off, such as the Panasonic SmartExhaust AirCycler combination fan/light timer control.

2.7.3 Replace Rooftop Air Handling Units

Outdoor rooftop air handling units have a life expectancy of approximately 20 years. The rooftop units are 14 years old and are in fair condition. They use R-22 refrigerant, an ozone-depleting chemical that has been phased out of production, making it expensive to replace or replenish when a failure occurs. Consider replacing these units in the next 5 years. Replacement units will not only use a more environmentally friendly refrigerant, they will be more energy efficient, and can use heat pump technology to minimize the use of natural gas.

This recommendation is an energy saving measure and does not increase the indoor air quality of the building, although the project could also address comfort issues and the ventilation issues noted in the following measure.

2.7.4 Add Ventilation to All Occupied Areas

Several corridors and other interior spaces do not have operable windows or any mechanical ventilation. Consider adding or extending the existing ventilation systems to serve these areas.

2.7.5 Install Split System Unit for Guard Office

The thermostat that controls RTU-5 serving the lockup area is located in the guard office, which has a substantial amount of heat-generating electronics. According to staff, the temperature is often adjusted manually because the holding cells are cold. Installing a mini-split to serve the guard office and relocating the existing thermostat would help improve comfort, but would not increase the indoor air quality.

2.8 Eastern Hampshire District Court Recommendations Checklist

Recommended Immediate Actions

1. □ 2.7.1: Run Supply Fans Continuously During Occupied Hours

Recommended Actions

- 2. ✓ RF-1: Replace filters with MERV-13
- 3. \Box RF-3: Install differential pressure sensors across the filter banks
- 4.
 □ RF-3a: Connect the pressure sensor to a local alarm
- 5. \checkmark RTB-1: Test and balance air handling unit airflow rates
- 6. □ RTB-5: Test and balance all air inlets and outlets
- 7. \Box RE-2: Clean air handler coils and drain pans
- 8.
 □ RC-1: Implement pre-occupancy flush sequence
- 9.
 □ RFC-1: Install portable HEPA filters

Other Actions

- 10. \Box 2.7.2: Repair or Replace Controls for Exhaust Fans
- 11.
 2.7.3: Replace Rooftop Air Handling Units
- 12. \Box 2.7.4: Add Ventilation to All Occupied Areas
- 13.
 □ 2.7.5: Install Split System Unit for Guard Office

Section 3 Testing & Balancing Results

Wing's Testing and Balancing Co. visited the Eastern Hampshire District Courthouse between November 27th and December 1st, 2021 to test the airflow rates of the air handling units and the exhaust fans. A summary of the tested airflow rates versus the design airflow rates are shown below in Tables 5 and 6. The full testing and balancing report is attached.

TABLE 5

Air Handler Airflow Testing & Balancing Results

		Design			Actual	
Unit	Total Supply Fan Airflow (CFM)	Recommended Outdoor Airflow (CFM)	Return Airflow (CFM)	Supply Fan Airflow (CFM)	Outdoor Airflow (CFM)	Return Airflow (CFM)
RTU-1	3,400	600	2,800	940	0	940
RTU-2	5,000	1,250	3,750	3,157	778	2,379
RTU-3	4,000	520	3,480	2,704	348	2,356
RTU-4	3,000	373	2,627	2,700	368	2,332
RTU-5	3,400	680	2,720	2,136	932	1,204
RTU-6	2,400	420	1,980	1,697	304	1,393
RTU-7	5,000	1,250	3,750	3,582	885	2,697
RTU-8	5,000	1,250	3,750	3,274	373	2,901

TABLE 6

Exhaust Fan T	Exhaust Fan Testing & Balancing Results								
Unit	Serving	Design Return/Exhaust Airflow (CFM)	Actual Return/Exhaust Airflow (CFM)						
Unit	Serving	(СГМ)	(СГМ)						
REF-1	Restrooms	400	651						
REF-2	Restrooms	400	908						
Lockup EF	Lockup	1,000	1,426						

The typical balancing tolerance for air systems is $\pm 10\%$ of the design airflow.

In reviewing the airflow report data, the following should be noted:

- 1. Only one out of eight rooftop units are providing acceptable supply airflow; most are performing well below the acceptable airflow range. Measured airflow rates outside of the 10% tolerance of the design airflow are shown in **boldface** in Tables 5 and 6.
- 2. The balancing contractor noted that the outdoor air intake screen for RTU-1 is "completely plugged and collapsing". Debris has likely built up on this screen so that the airway is completely blocked and no measurable outdoor air is entering the unit. We recommend clearing and/or replacing that screen and rebalancing the outdoor airflow to this unit.
- 3. RTUs 2, 3, 5, 6, 7, and 8 are all operating well below the design airflow rates due to low fan speed. The average shortfall is almost 40%, which seems to be solely related to upgrading the filters to MERV-13. We strongly recommend changing the sheaves for these rooftop units in order to reach design airflow rates.
- 4. The balancing contractor noted that the outdoor air damper actuators for RTU-5 and RTU-8 are not operational. We recommend repairing or replacing these actuators, and rebalancing the outdoor airflows when the supply airflows are addressed.
 - a. The outdoor airflow percentage for RTU-5 was more than double the recommended value. This may result in the unit not being able to provide adequate supply air temperatures during peak weather conditions.
 - b. The outdoor airflow percentage for RTU-8 was less than half the recommended value.
- 5. It appears that two of the rooftop exhaust fans were provided with high-flow impellers (model 90ACEH) rather than low-flow as specified (model 90C15DL on the plans). The three rooftop exhaust fans are all running significantly above their design airflow rates, developing a negative pressure in the spaces they serve. While it is normal for restrooms and lockup areas to be slightly negatively pressurized, this is of greater concern because most RTUs are not providing the design levels of outdoor airflow. Exhaust airflow beyond design levels will cause excess energy use for cooling and heating, so this should be addressed when operation changes to post-pandemic conditions. Our recommendations are to first address the shortfall in outdoor air, and then rebalance exhaust airflows when "normal" operation resumes.

Disclaimer

Tighe and Bond cannot in any way guarantee the effectiveness of the proposed recommendations to reduce the presence or transmission of viral infection. Our scope of work is intended to inform the Office of Court Management on recommendations for best practices based on the guidelines published by ASHRAE and the CDC. Please note that these recommendations are measures that may help reduce the risk of airborne exposure to COVID-19 but cannot eliminate the exposure or the threat of the virus. Implementing the proposed recommendations will not guarantee the safety of building occupants. Tighe & Bond will not be held responsible should building occupants contract the virus. The Office of Court Management should refer to other guidelines, published by the CDC and other governing entities, such as social distancing, wearing face masks, cleaning and disinfecting surfaces, etc. to help reduce the risk of exposure of COVID-19 to building occupants.

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Eastern Hampshire District Court HVAC Ventilation Survey

* * * *

Tighe & Bond Attn: Jason Urso 53 Southampton Road Westfield, MA 01085

December 1st, 2021



December 1st, 2021

Tighe and Bond Attn: Jason Urso 53 Southampton Road Westfield, MA 01085

Re: Eastern Hampshire District Court HVAC Ventilation Survey

Dear, Jason

Wing's has completed the HVAC Survey for the above referenced location. Upon arrival it was noted that all filters are MERV-13 rated. The heating on the units is gas and the cooling side is Dx. There are several single restroom EFs that are tied into the light switches and are only on when the restroom is occupied. The results of our testing are as follows:

- The outside air louver screen for RTU-1 is completely plugged and collapsing. It needs to be replaced.
- RTUs 2, 3, 4, 5, 6, 7 and 8 all need sheave changes to speed them up.
- RTUs 5 and 8 have outside air actuators that are broken and need replacing.
- The exhaust fans all check out with no issues.

The following pages are your record of current operating conditions. If you have any questions, or if we can be of further service, please do not hesitate to call.

Very truly yours,

Wing's Testing & Balancing Co., Inc.

ICB Certified Contractor for: TABB—Commissioning—Fire/Life Safety L1&L2—Sound & Vibration

Barry Stratos Certified TABB Technician CT SM-2 License 6386 MA SM-2 13595



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ROJECT: Eastern Hamp	shire District Co	ourt		12 Mar 100 1	DATE:	11/27/21
REA SERVED: RTUs					TECH: BS	
		FAN DA	TA			
FAN NUMBER	RT	U-1	RTU	-2 (2)	RTU-	3 (2)
LOCATION	Rc	oof	Roof		Roof	
AREA SERVED	Room 73+165		Offices		Conference 105	
MANUFACTURER	Trane		Trane		Trane	
MODEL OR SIZE	YHC10	2A3RH	YCD1	51C3H	YHC12	0A3RL
	DESIGN	ACTUAL	DESIGN	ACTUAL	DESIGN	ACTUAL
TOTAL CFM	3400	940	5000	3157	4000	2704
RETURN AIR	2800		3750	2379	3480	2356
OUTSIDE AIR	600	(1)	1250	778	520	348
DISCH. STATIC		+0.22"		+0.14"		+0.64"
SUCTION STATIC		-1.23"		-0.60''		-1.15"
TOTAL STATIC		1.45"		0.74"		1.79"
FAN RPM		870		725		1009
PULLEY O.D.	6.0" x 1		8.5" x 1		5.5" x 1	
ESP	1.16		0.53		1.04	
VFD SPEED	No VFD		No VFD		No VFD	
O.A.D.MIN POS	NA		10%		5%	
		MOTOR	ΔΤΔ			
MANUFACTURER	G	iΕ		6E	G	E
MODEL OR FR.		5T	56 Hz		56 Hz	
HORSEPOWER	2	2	3	3	3	3
MOTOR RPM	1725	1725	1725	1725	1725	1725
VOLTAGE / PH.	208/3	208/3	208/3	208/3	208/3	208/3
LEG 1	6.3	5.2	9.4	6.4	9.4	7.4
AMPS LEG 2		5.2		6.4		7.5
LEG 3		5.2		6.4		7.4
SHEAVE O.D.	3.75"	x 7/8	4.0"	x 7/8	4.25"	
BELTS - QUANTITY / SIZE		435		X62	the second se	\35
SHEAVE POSITION		Open		Open		Open
C to C		l.5		L.O		
	1					

(2) Unit needs sheave change to speed up.

NA Not Available | ND No Design | DD Direct Drive | N/R No Requirement

ROJECT: Eastern Har	npshire District C	ourt			DATE:	11/30/21	
REA SERVED: RTUs					TECH:	BS	
		FAN DA	ATA				
FAN NUMBER		U-4	RT	U-5	RTU	-6 (1)	
LOCATION		oof	Roof		Roof		
AREA SERVED		ounge	Lock-Up		Offices		
MANUFACTURER	and a second	Trane		ane	Tra	ane	
MODEL OR SIZE		YHC120A3RL		2A3RH	YHCO7	2A3RM	
	DESIGN	ACTUAL	DESIGN	ACTUAL	DESIGN	ACTUAL	
TOTAL CFM	3000	2700	3400	2136	2400	1697	
RETURN AIR	2627	2332	2720	932	1980	1393	
OUTSIDE AIR	373	368	680	1204 (2)	420	304	
DISCH. STATIC		+1.05"		+1.02"		+0.25"	
SUCTION STATIC		-0.64''		-0.51''		-0.51"	
TOTAL STATIC		1.64		1.53''			
FAN RPM		906		929		851	
PULLEY O.D.		'x1	5.5	"×1	6.0'	" x 1	
ESP		40	1.	1.20		53	
VFD SPEED O.A.D.MIN POS		No VFD		No VFD		No VFD	
		%		0%		%	
		MOTOR	ΟΑΤΑ				
MANUFACTURER		MOTOR I		5E	G	5E	
MODEL OR FR.		ie ST	G	GE IST		БЕ Hz	
MODEL OR FR. HORSEPOWER	14 2	iE -5T 2	G				
MODEL OR FR. HORSEPOWER MOTOR RPM	14 2 1725	ie ST	14	IST	56	Hz	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH.	14 2 1725 208/3	E 5T 2 1725 208/3	0 14 2	5T 2	56 1	Hz 1	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1	14 2 1725	E 5T 2 1725 208/3 6.1	0 14 2 1725	2 1725	56 1 1725	Hz 1 1725	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2	14 2 1725 208/3	E 5T 2 1725 208/3 6.1 6.1	2 1725 208/3	2 1725 208/3	56 1 1725 208/3	Hz 1 1725 208/3	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2 LEG 3	14 2 1725 208/3 6.3 	E 5T 2 1725 208/3 6.1 6.1 6.1 6.1	2 1725 208/3 6.5 	2 1725 208/3 5.8 5.8 5.8 5.8	56 1 1725 208/3 5.0	Hz 1 1725 208/3 3.4	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2 LEG 3 SHEAVE O.D.	14 2 1725 208/3 6.3 3.75"	E 5T 2 1725 208/3 6.1 6.1 6.1 x 7/8	2 1725 208/3 6.5 3.5"	2 1725 208/3 5.8 5.8 5.8 5.8 x 3/4	56 1 1725 208/3 5.0 3.5"	Hz 1725 208/3 3.4 3.4 3.4 3.4 x 5/8	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2 LEG 3 SHEAVE O.D. BELTS - QUANTITY / SIZE	14 2 1725 208/3 6.3 3.75" 1/A	E 5T 2 1725 208/3 6.1 6.1 6.1 x 7/8 X35	00000000000000000000000000000000000000	2 1725 208/3 5.8 5.8 5.8 5.8 x 3/4 X35	56 1 1725 208/3 5.0 3.5"	Hz 1 1725 208/3 3.4 3.4 3.4 3.4	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2 LEG 3 SHEAVE O.D. BELTS - QUANTITY / SIZE SHEAVE POSITION	14 2 1725 208/3 6.3 3.75" 1/A 1/2 0	E 5T 2 1725 208/3 6.1 6.1 6.1 x 7/8 X35 Dpen	14 2 1725 208/3 6.5 3.5" 1/A 1/2 0	2 1725 208/3 5.8 5.8 5.8 5.8 x 3/4 X35 Dpen	56 1 1725 208/3 5.0 3.5" 1/A	Hz 1 1725 208/3 3.4 3.4 3.4 3.4 x 5/8	
MODEL OR FR. HORSEPOWER MOTOR RPM VOLTAGE / PH. LEG 1 AMPS LEG 2 LEG 3 SHEAVE O.D. BELTS - QUANTITY / SIZE	14 2 1725 208/3 6.3 3.75" 1/A 1/2 0	E 5T 2 1725 208/3 6.1 6.1 6.1 x 7/8 X35	14 2 1725 208/3 6.5 3.5" 1/A 1/2 0	2 1725 208/3 5.8 5.8 5.8 5.8 x 3/4 X35	56 1 1725 208/3 5.0 3.5" 1/A Fully	Hz 1725 208/3 3.4 3.4 3.4 3.4 x 5/8 X35	

(1) Unit needs sheave change to speed up.

(2) OA actuator broken and needs to be replaced.

NA Not Available | ND No Design | DD Direct Drive | N/R No Requirement

	oshire District Co	ourt			DATE:	11/29/21
REA SERVED: RTUs					TECH:	BS
		FAN DA				
FAN NUMBER	RTU-	Contraction of the local data and the local data an	and the second se	-8 (1)		
LOCATION	Ro		Roof			
AREA SERVED	Cou	Contraction of the second s		rt #2		
MANUFACTURER	Trane			ane		
MODEL OR SIZE	YCD15			51C3H		
	DESIGN	ACTUAL	DESIGN	ACTUAL	DESIGN	ACTUAL
TOTAL CFM	5000	3582	5000	3274		
RETURN AIR	3750	2697	3750	2901		
OUTSIDE AIR	1250	885	1250	373 (2)		
DISCH. STATIC		+0.22"		+0.27"		
SUCTION STATIC		-0.68''		-0.67"		
TOTAL STATIC		0.90		0.94''		
FAN RPM		762		763		
PULLEY O.D.	8.5'			'x1		
ESP	0.			0.62		
VFD SPEED O.A.D.MIN POS	No VFD 20%		No VFD 0%			
			0	70		
		MOTOR				
MANUFACTURER	G		GE			
MODEL OR FR.		Hz	56 Hz			
HORSEPOWER	3	3	3	3		
MOTOR RPM	1725	1725	1725	1725		
VOLTAGE / PH.	208/3	208/3	208/3	208/3		
LEG 1	9.4	7.1	9.4	7.0		
AMPS LEG 2		7.1		7.0		i
LEG 3		7.1		7.0		
SHEAVE O.D.	4.25"			x 7/9		
BELTS - QUANTITY / SIZE		362		363		
SHEAVE POSITION		Dpen		losed		
C to C	21	0	21	1.0		
		REMAR				

(2) OA actuator broken and needs to be replaced.

NA Not Available | ND No Design | DD Direct Drive | N/R No Requirement

PROJECT: Eastern Hampshire District Court							DATE:				
AREA SERVED:	RTUs	TECH:									
TRAVERSE		AREA	DESIGN		CENT. STAT.	TE					
LOCATIONS	DUCT SIZE "	SQ.FT.	FPM	CFM	PRESS."	FPM	CFM	NOTE			
RTU-1 Total	36" x 16"	4.0		3400	Velgrid	225	940				
RTU-1 OA	36" x 16"	4.0		600	Velgrid			1			
RTU-1 Return				2800	Calculated						
RTU-2 Total	48" x 16"	5.33		5000	Velgrid	592	3157				
RTU-2 OA	48" x 16"	5.33		1250	Velgrid	146	778				
RTU-2 Return				3750	Calculated		2379				
RTU-3 Total	36" x 16"	4.0		4000	Velgrid	676	2704				
RTU-3 OA	36" x 16"	4.0		520	Velgrid	87	348				
RTU-3 Return				3480	Calculated		2356				
RTU-4 Total	36" x 16"	4.0		3000	Velgrid	675	2700				
RTU-4 OA	36" x 16"	4.0		373	Velgrid	92	368				
RTU-4 Return				2627	Calculated		2332				
RTU-5 Total	36" x 16"	4.0		3400	Velgrid	534	2136				
RTU-5 OA	36" x 16"	4.0		680	Velgrid	301	1204	(2)			
RTU-5 Return				2720	Calculated		932	(2)			
RTU-6 Total	36" x 16"	4.0		2400	Velgrid	424	1697				
RTU-6 OA	36" x 16"	4.0		420	Velgrid	76	304				
RTU-6 Return				1980	Calculated		1394				
RTU-7 Total	48'' x 16''	5.33		5000	Velgrid	627	3582				
RTU-7 OA	48" x 16"	5.33		1250	Velgrid	166	885				
RTU-7 Return				3750	Calculated		2697				
RTU-8 Total	48'' x 16''	5.33		5000	Velgrid	614	3274				
RTU-8 OA	48" x 16"	5.33		1250	Velgrid	70	373				
RTU-8 Return				3750	Calculated		2901				
and the second second second second	AND	Section 1	REN	ARKS	STREET, STREET,		Sectors in	SCHEROLAN ST			

(1) Outside air intake screen is completely clogged and collapsing and needs to be replaced.(2) OA actuator broken and needs to be replaced.

PROJECT:	Eastern Hampshi	DATE: 12/01/21			
AREA SERVED:	REFs	TECH: BS			
		FAN D	ATA	Server and a server	
FAN NUMBER		REF-1	REF-2	Lock Up EF	
LOCATION		Roof	Roof	Roof	
AREA SERVED		Restrooms	Restrooms	Lock-Up	
MANUFA	CTURER	Cook	Cook	Cook	
MODEL	OR SIZE	90ACEH	90ACEH	90ACEH	
TOTAL CFM	DESIGN	400	400	1000	
	ACTUAL	651	908	1426	
	DESIGN	1550	1550	1550	
FAN RPM	ACTUAL	1550	1550	1550	
ULLEY	0.D.	DD	DD	DD	
SERV					
and Salarahar and		MOTOR	DATA		
MANUFACTURER		Fasco	Fasco	Fasco	
MODEL NUMBER			*		
MOTOR HP	DESIGN	1/8	1/8	1/4	
	ACTUAL	1/8	1/8	1/4	
MOTOR RPM		1550	1550	1550	
VOLTAGE	/PHASE	115/1	115/1	115/1	
	DESIGN	1.7	1.7	3.2	
	ACT. LEG 1				
MOTOR AMPS	ACT. LEG 2	1.5	1.8	3.3	
	ACT. LEG 3				
SHEA		DD	DD	DD	
BELTS - QUANTITY/SIZE		DD	DD	DD	
SHEAVE POSITION		DD	DD	DD	
		REMA	RKS		

PROJECT: Eastern Hampshire District Court								DATE: 12/01/21			
SYSTEM / AREA:	REFs							TECH: BS			
LOCATION	a weather	100000000000000000000000000000000000000	AK	DESIGN		TEST		FINAL		Second Second	
	NO.	SIZE		FPM	CFM	FPM	CFM	FPM	CFM	NOTES	
REF-1										1	
Men's Room		10'' x 10''	0.50	400	200	668	334				
Women's Room		10" x 10"	0.50	400	200	634	317				
					400		651				
REF-2	_										
Restroom 183		8" x 8"	0.32		100	520	260				
Restroom 184		8" x 8"	0.32		100	494	247				
Restroom 185	_	8" x 8"	0.32		100	459	230				
Restroom 186		8" x 8"	0.32		100	342	171				
	_				400		908				
Lock-Up EF											
Cell 1	_	7" x 7"	0.34		143	641	217				
Cell 2		7" x 7"	0.34		143	606	206				
Cell 3		7" x 7"	0.34		143	762	208				
Cell 4		7" x 7"	0.34		143	589	200				
Cell 1B		7" x 7"	0.34		143	676	200				
Cell 2B		7" x 7"	0.34		143	446	152				
Cell C		7" x 7"	0.34		143	475	162				
			0.01		1000	475	1426				
							1120				
				1.55)							
					ARKS						